

# Photocathodes for ultra high-gradient NCRF guns

Gerard Lawler et al.



# Outline of presentation

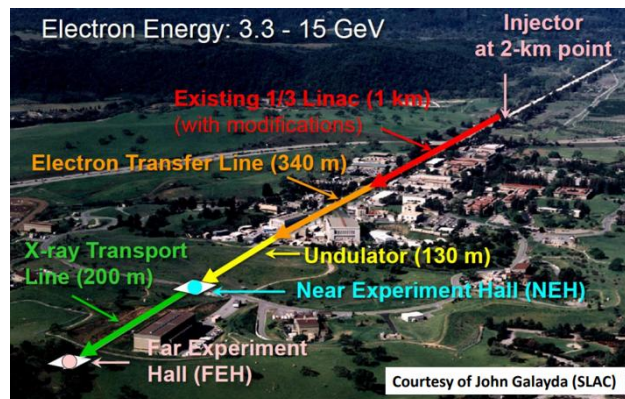
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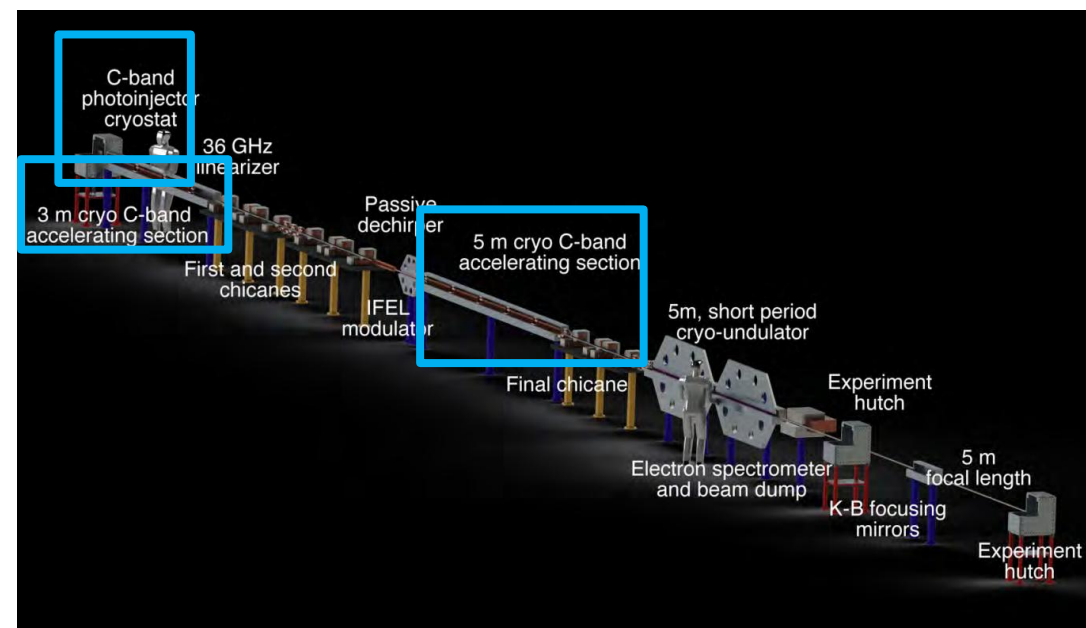
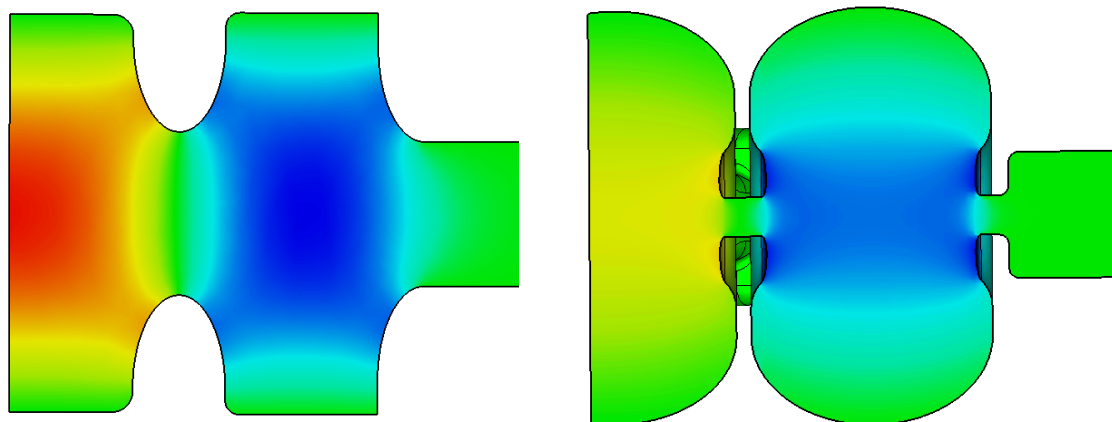
1. Background and motivation
2. Electron emission considerations
3. Experimental results
4. Temperature dependence
5. Future directions
6. Conclusions



- Our most pertinent realization of high gradient and high brightness techniques is Ultra-Compact Xray FEL (UCXFEL) concept (right)
- When combined with novel bunching and short period undulators we can approach 40m scales with several applications incl. allowing university scale XFEL access and chip metrology
- Existing plan incorporates cryogenically enabled  $>200$  MV/m photoinjector peak fields and  $\approx 70$  MV/m linacs



J. Galayda et al., "The new lcls-ii project: Status and challenges," in LINAC, 2014, pp. 404–408. [Online]. Available: [https://accelconf.web.cern.ch/linac2014/talks/tuioa04\\_talk.pdf](https://accelconf.web.cern.ch/linac2014/talks/tuioa04_talk.pdf).



Rosenzweig, J. B. et al., *New Journal of Physics*, vol. 22, no. 9, p. 093067, 2020. doi:10.1088/1367-2630/abb16c

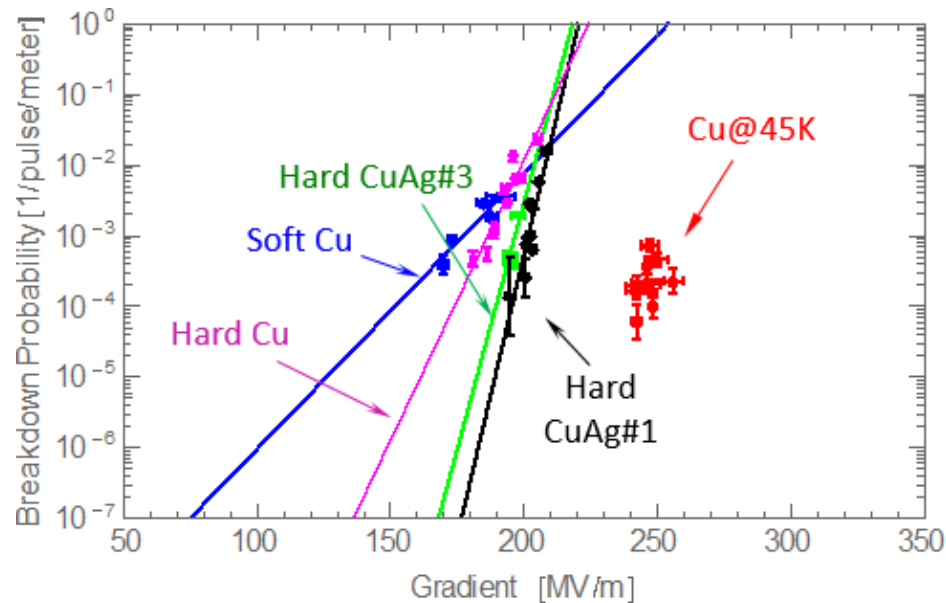


# Cryogenic photogun brightness

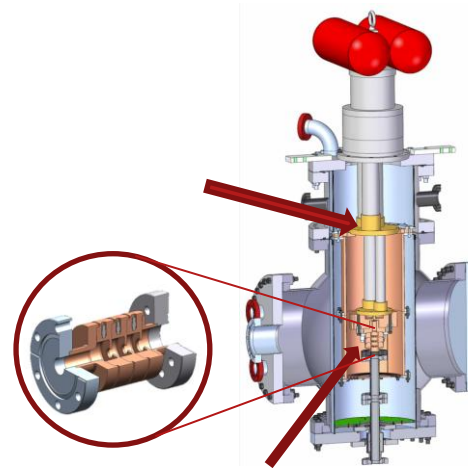


- Limit to high gradient often breakdown rate (BDR)
- SLAC cryogenic breakdown reduction  $\Rightarrow$  higher accelerating gradients possible
- 1D space charge limited brightness scaling
  - Note launch field and temperature dependence
- *TopGun* previous development in S-band

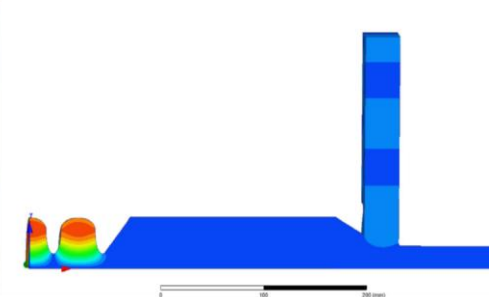
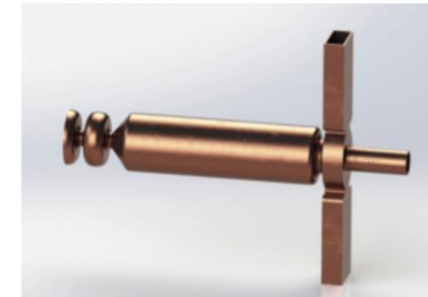
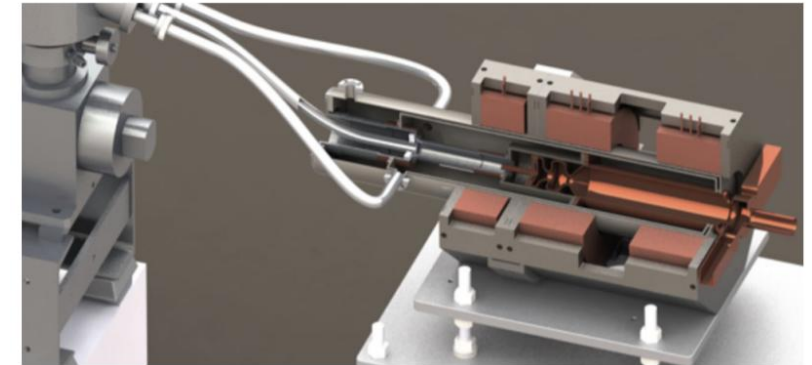
Rosenzweig, J. B., et al. *Physical Review Accelerators and Beams* 22.2 (2019): 023403.  
Doi: 10.1103/PhysRevAccelBeams.22.023403%7



$$B_{e,b} \approx \frac{2ec\epsilon_0}{k_B T_c} (E_0 \sin \varphi_0)^2$$



Cavities for high power test





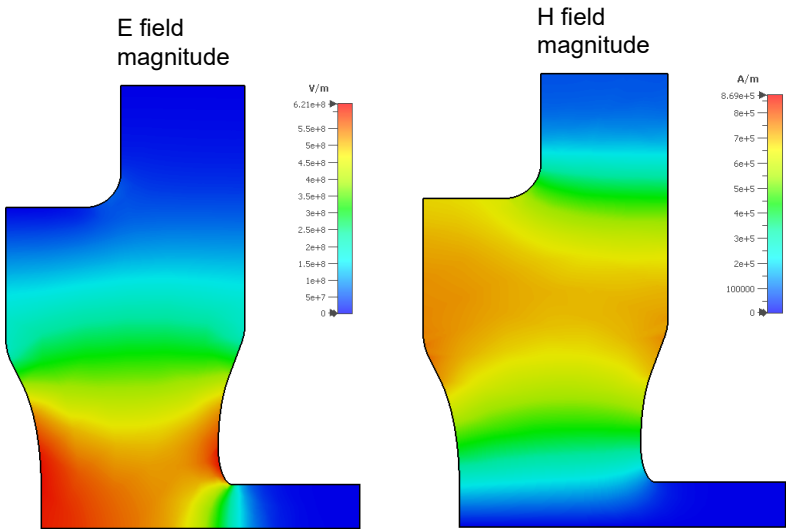
# Cryo RF Performance Overview



- Parameters for gun thus far compared to RRR100-500 case (left) with empirical numbers measured to inform simulations (right)

Parameter	295K	100K	77K	40K
Frequency	5.695 GHz	5.711 GHz	5.712 GHz	5.713 GHz
$Q_0$	8579	18668	24200	39812
$\beta$	0.7	1.53	1.98	3.26
Filling time	-	0.41 $\mu$ s	0.45 $\mu$ s	0.52 $\mu$ s

Lawler, G. E., et al. *Instruments* 8.1 (2024): 14.  
Doi: 10.3390/instruments8010014



Parameter	295 K	95 K	77K	45 K
$f_0$ [MHz]	$5703.6 \pm 0.1^1$	$5720.410 \pm 0.003^1$	$5721 \pm 3$	$5722 \pm 4$
$Q_0$	$7808 \pm 13^1$	$14326 \pm 12^1$	$21000 \pm 3600$	$30000 \pm 9900$
Coupling $\beta$	$0.608 \pm 0.002^1$	$1.069 \pm 0.002^1$	$1.60 \pm 0.44$	$2.4 \pm 0.9$
Filling time [ $\mu$ s]	$0.271 \pm 0.01^1$	$0.386 \pm 0.001^1$	$0.44 \pm 0.01$	$0.49 \pm 0.03$
Power [MW] for 120 MV/m	$1.23 \pm 0.10$	$0.85 \pm 0.08$	$0.79 \pm 0.01$	$0.70 \pm 0.09$
Energy [J] per 2 $\mu$ s pulse	$2.45 \pm 0.01$	$1.70 \pm 0.02$	$1.58 \pm 0.03$	$1.40 \pm 0.19$
Cathode field @ 0.5 MW	$77 \pm 3$ MV/m	$92 \pm 5$ MV/m	$93 \pm 3$ MV/m	$102 \pm 7$ MV/m

<sup>1</sup> Values experimentally measured or computed directly from low power measurements



# Gun Comparisons



- CYBORG design inspired primarily by 3 existing photoguns: PEGASUS; Cornell Cryo DC gun; FERMI
- Compared CYBORG design specs also with existing cathode test beds

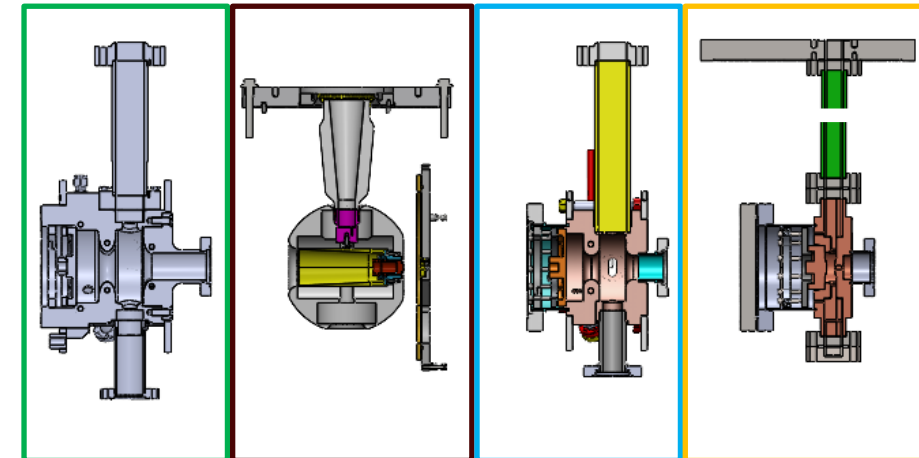
Parameter	CYBORG Phase 1	CYBORG Phase 2
Cavity type	normal conducting	-
Cavity geometry	$\frac{1}{2}$ -cell reentrant	-
Cathode Assembly	Demountable Cu backplate	Cryogenic load lock
Design frequency	5.712 GHz	5.700 – 5.720 GHz
Peak cathode field	$\geq 120$ MV/m	-
Operating temperature	300 – 95K <sup>1</sup>	300 – 77K

<sup>1</sup> Current lowest temperature achieved with additional plans for 77 K operation

Photoguns	FERMI [20]	PEGASUS [6,21]	PITZ [22,23]	HZDR [24]/HZB [25]	Cornell [26]/ASU [27]	BNL [25,28]
Cavity type *	NCRF	NCRF	NCRF	SRF	-	SRF
Cavity geometry *	1.6 cell pillbox	1.6 cell pillbox	1.5 cell pillbox	1.5 cell elliptical	-	quarter wave
Cathode assembly	Demountable Cu backplate	Demountable Cu backplate + load-lock	Demountable Cu backplate + load-lock	Load-lock	Load-lock	Load-lock
Design frequency	2.998 GHz	2.856 GHz	1.3 GHz	1.3 GHz	DC	0.113 GHz
Peak cathode field	125 MV/m	120 MV/m (Cu backplate)	60 MV/m	15 – 20 MV/m	10 MV/m	10 – 15 MV/m
Min cathode T	$\geq$ room T	$\geq$ room T	$\geq$ room T	80 K	35 K	2 K

\* Only relevant for RF guns.

Lawler, G. E., et al. *Instruments* 8.1 (2024): 14.  
Doi: 10.3390/instruments8010014







# Dark current simulations

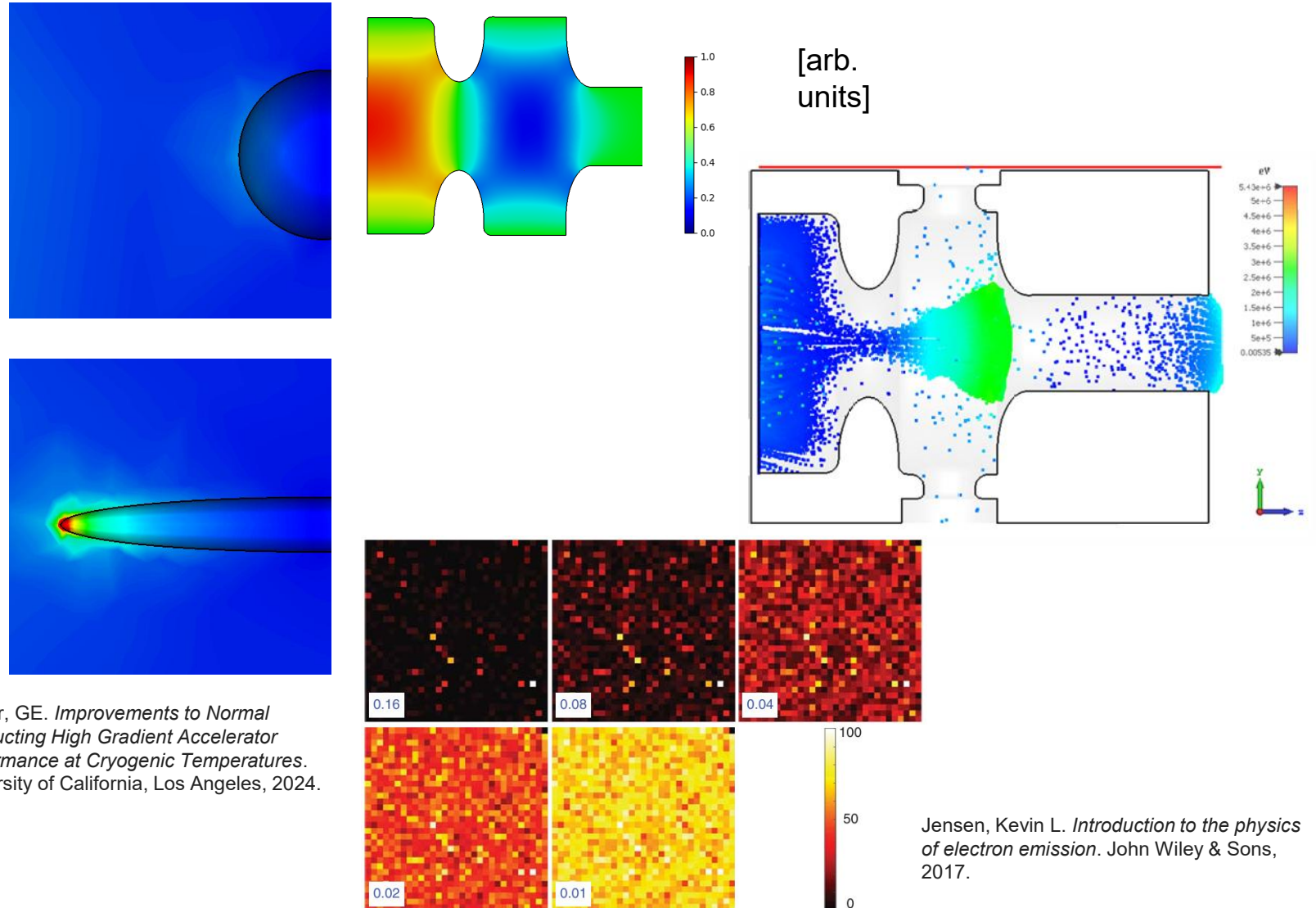


- Fowler-Nordheim field emission in particle-in-cell (PIC) simulation via CST with peak cathode plane gradient 60 MV/m and  $\beta = 50$  needed for significant emission
- Further uniformity assumption

$$J_F(F) = \frac{A_0}{\Phi t_0^2} \left( \frac{\Phi^2 e^6}{4Q} \right)^v F^{2-v} \exp \left( \frac{-B_0 \Phi^{3/2}}{F} \right)$$

Lawler, GE. *Improvements to Normal Conducting High Gradient Accelerator Performance at Cryogenic Temperatures*. University of California, Los Angeles, 2024.

R. N. Allan and A. J. Salim, "Prebreakdown currents and breakdown voltages in vacuum at cryogenic temperatures," *Journal of Physics D: Applied Physics*, vol. 7, no. 8, p. 1159, May 1974. doi: 10.1088/0022-3727/7/8/313



Jensen, Kevin L. *Introduction to the physics of electron emission*. John Wiley & Sons, 2017.

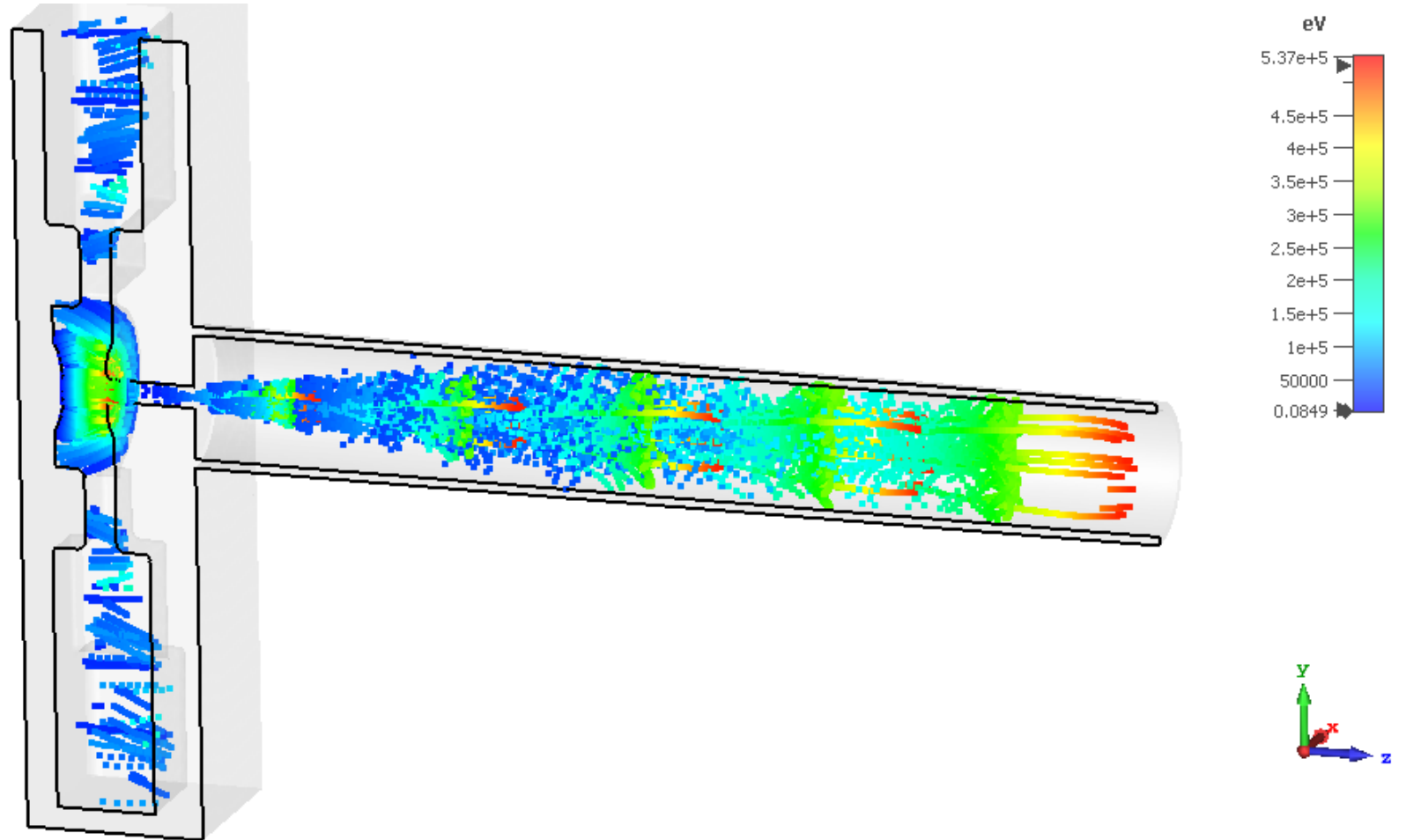


# Dark current simulation



- Fowler-Nordheim field emission in particle-in-cell (PIC) simulation via CST with peak cathode plane gradient 60 MV/m and  $\beta = 50$  needed for significant emission
- Further uniformity assumption
- Increased capture in  $\frac{1}{2}$  cell reentrant geometry

$$J_F(F) = \frac{A_0}{\Phi t_0^2} \left( \frac{\Phi^2 e^6}{4Q} \right)^v F^{2-v} \exp \left( \frac{-B_0 \Phi^{3/2}}{F} \right)$$



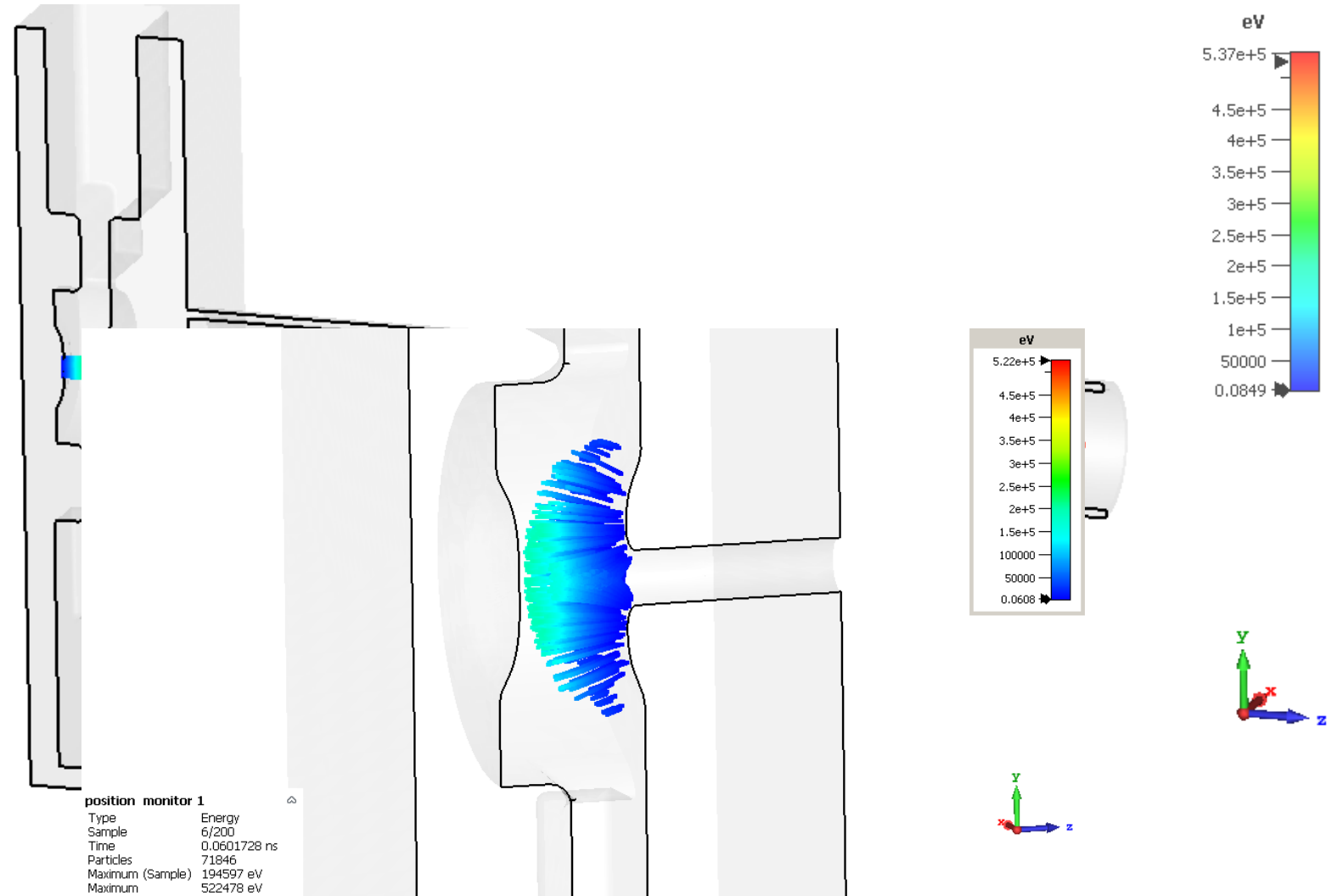




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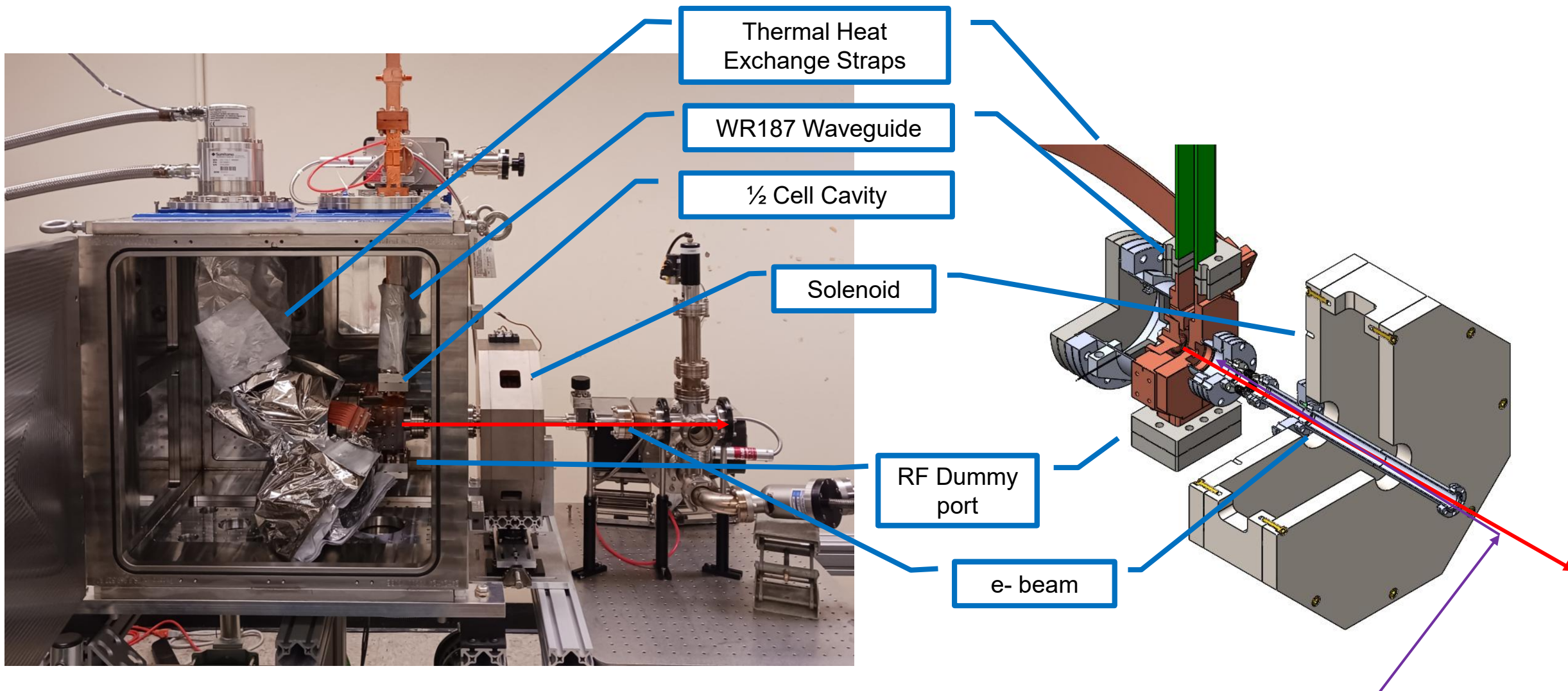


- Considering peak electric field enhancement optimized on nosecone, down stream dark current emission mostly localized to nosecone
- Isolated nosecone emission (right) showing additional collimation from iris and beam pipe





# CYBORG Phase1

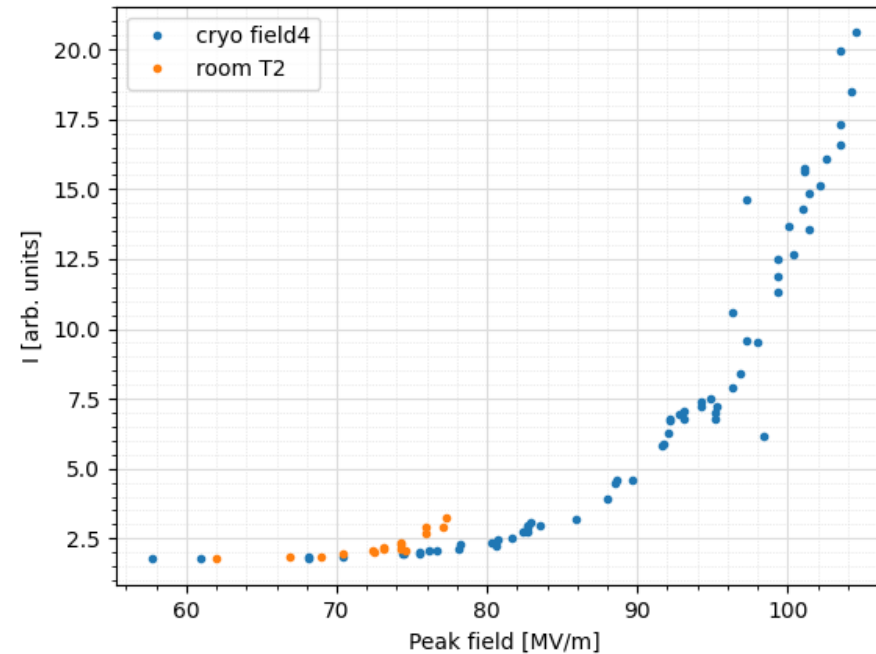
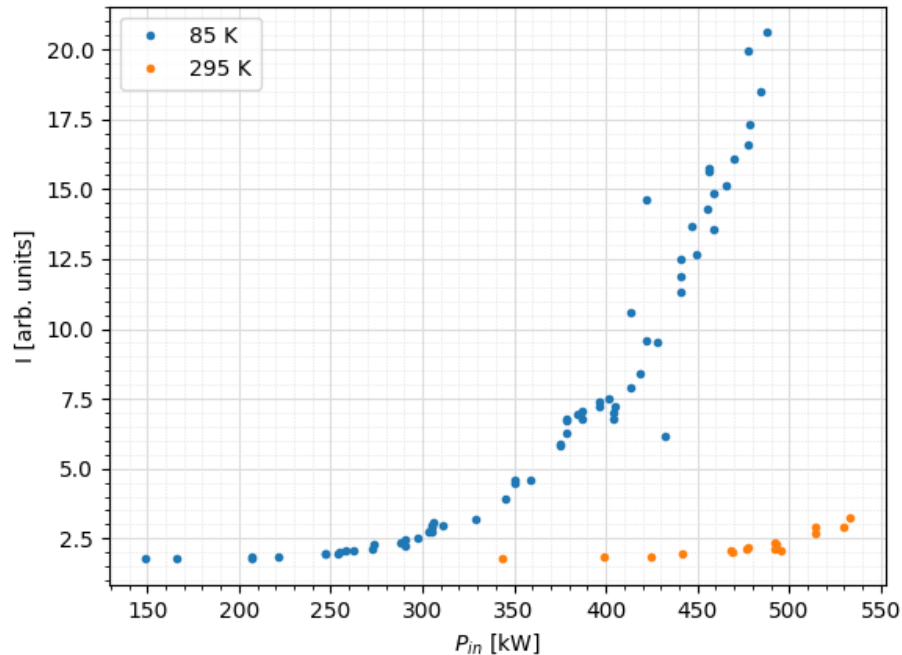




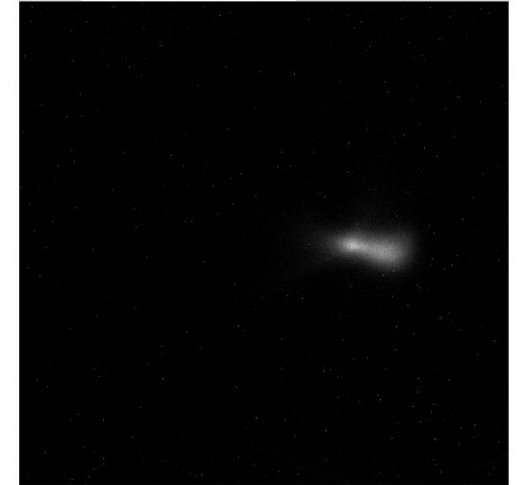
# Peak RF Performance



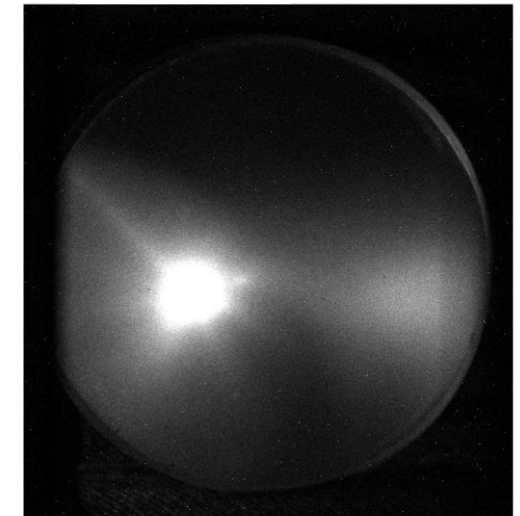
- Maximum RF input power currently into gun between 450 – 520 kW with fluctuation, stable at 450 kW
- Max peak field estimate >90 MV/m at 85K and 78 MV/m at room temperature
  - Determined with two different methods reflected pulse QL calculation and using coupling + Q0 from low power test
- Plots below show dark current scaling which show significant improvement of field possible using same input RF power
- YAG screen dark current measurements at approximately same input power



70 MV/m @ 295 K



95 MV/m @ 82.5 K

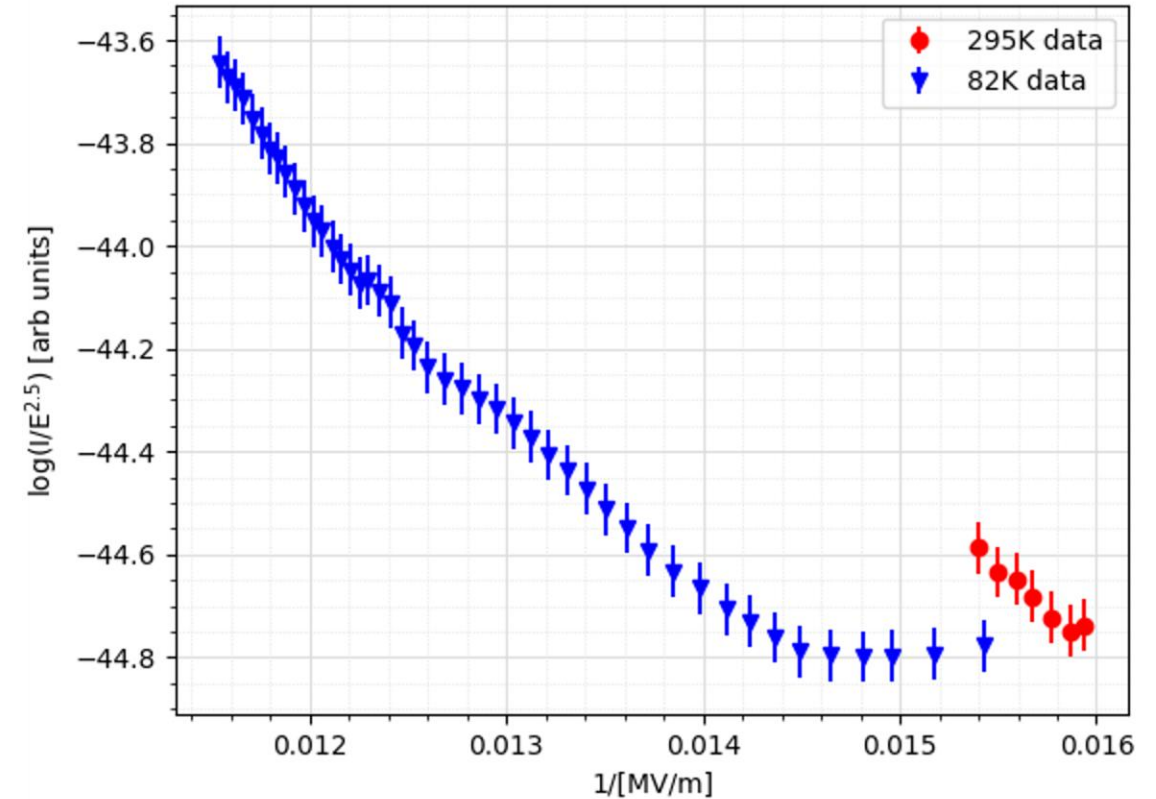
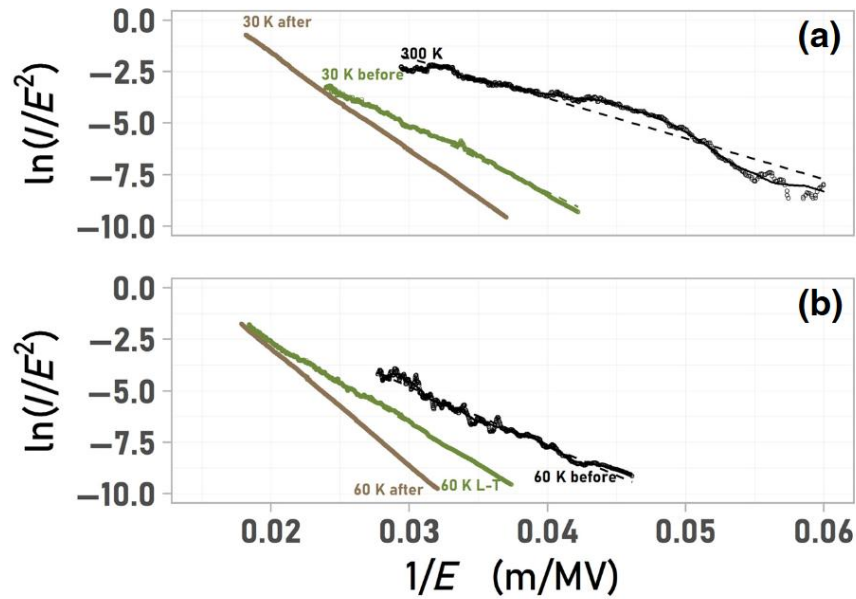




# Dark current temperature dependence



- Cryogenic pulsed DC experiments show temperature dependence (below)
- Begun to see similar results in CYBORG during high field conditioning (right)



Jacewicz, Marek, et al. "Temperature-dependent field emission and breakdown measurements using a pulsed high-voltage cryosystem." *Physical Review Applied* 14.6 (2020): 061002.

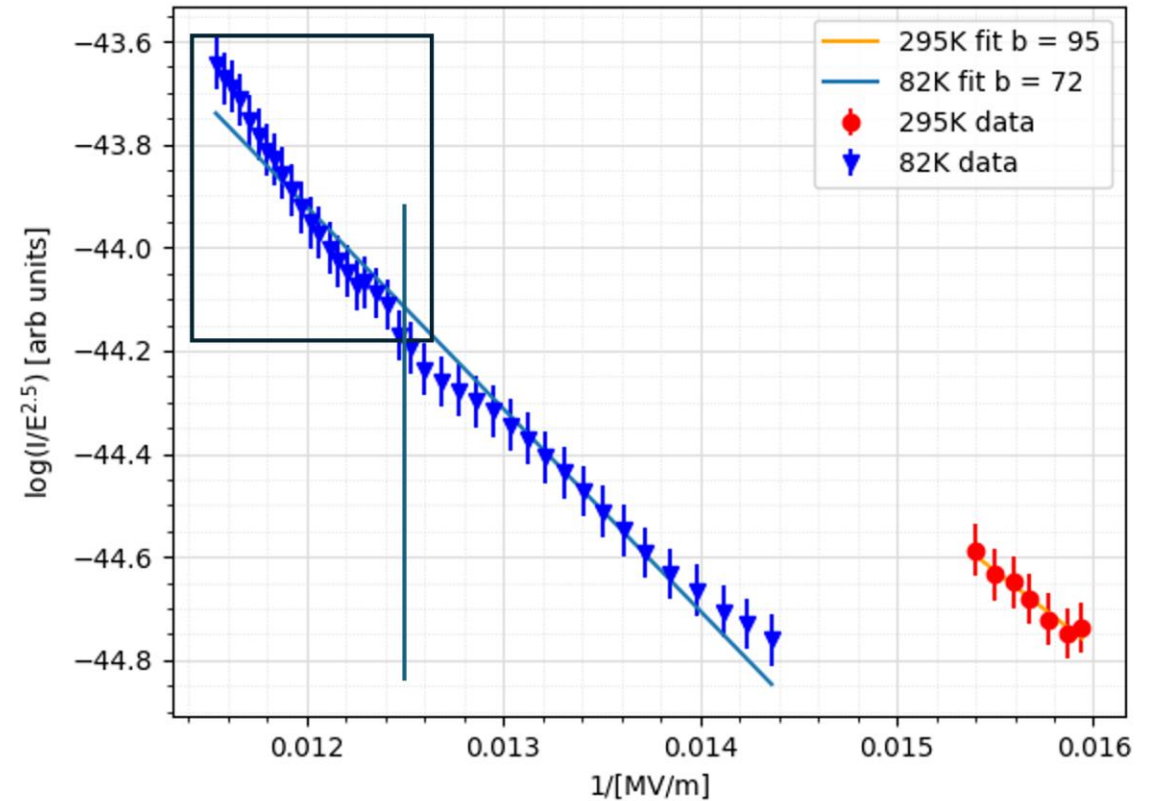
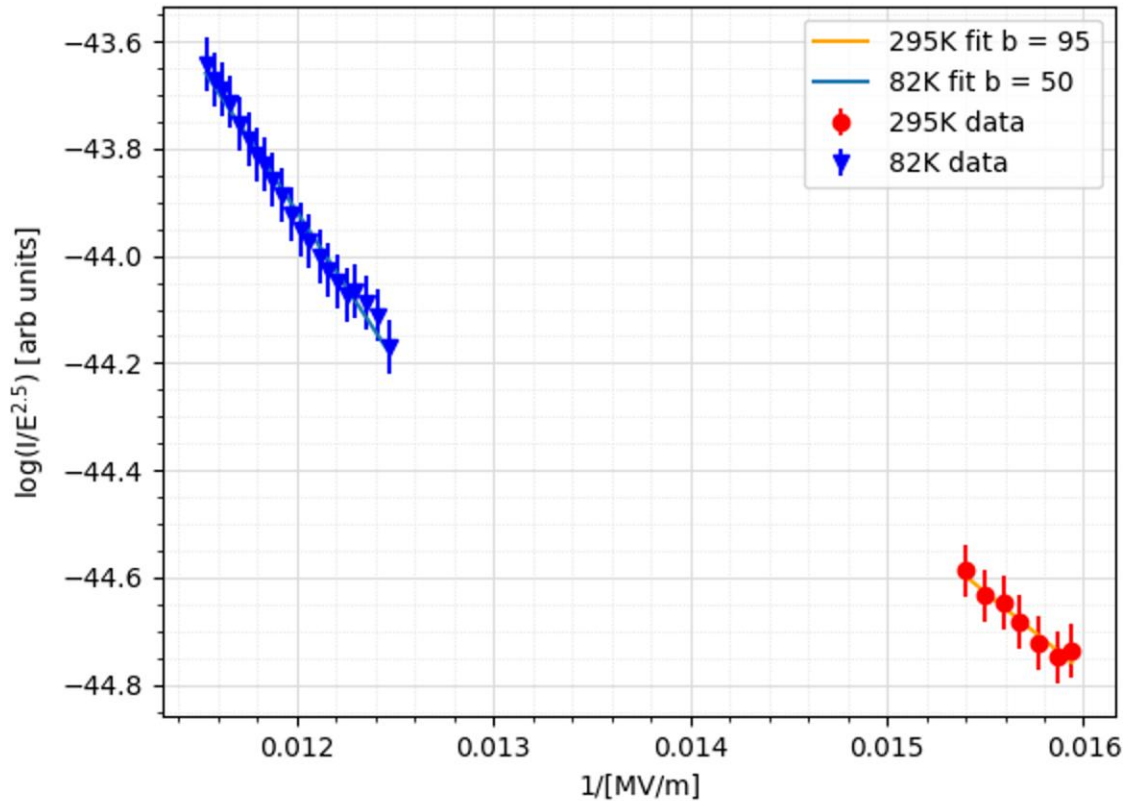




# Dark current temperature dependence



- Effective enhancement appears reduced for higher fields
- Data has implicit time dependence on scale of hours at 1 Hz rep rate so may represent also an effect of conditioning
- More data needed



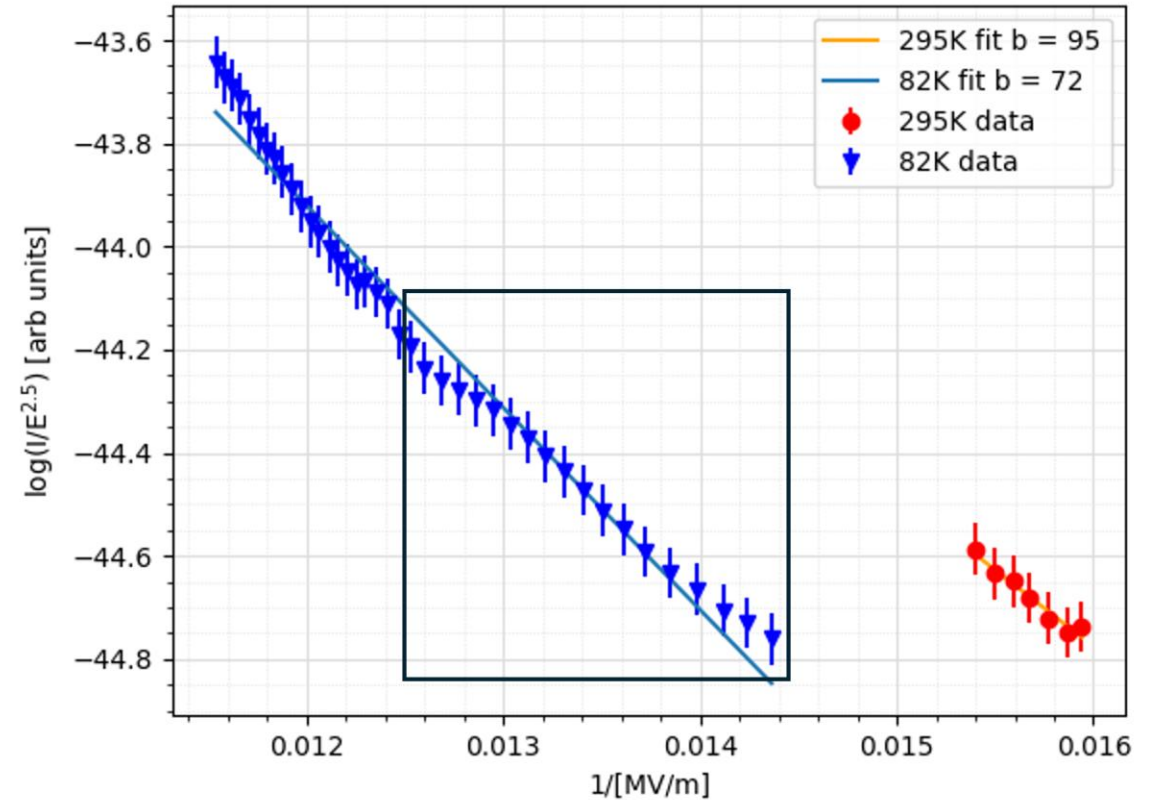
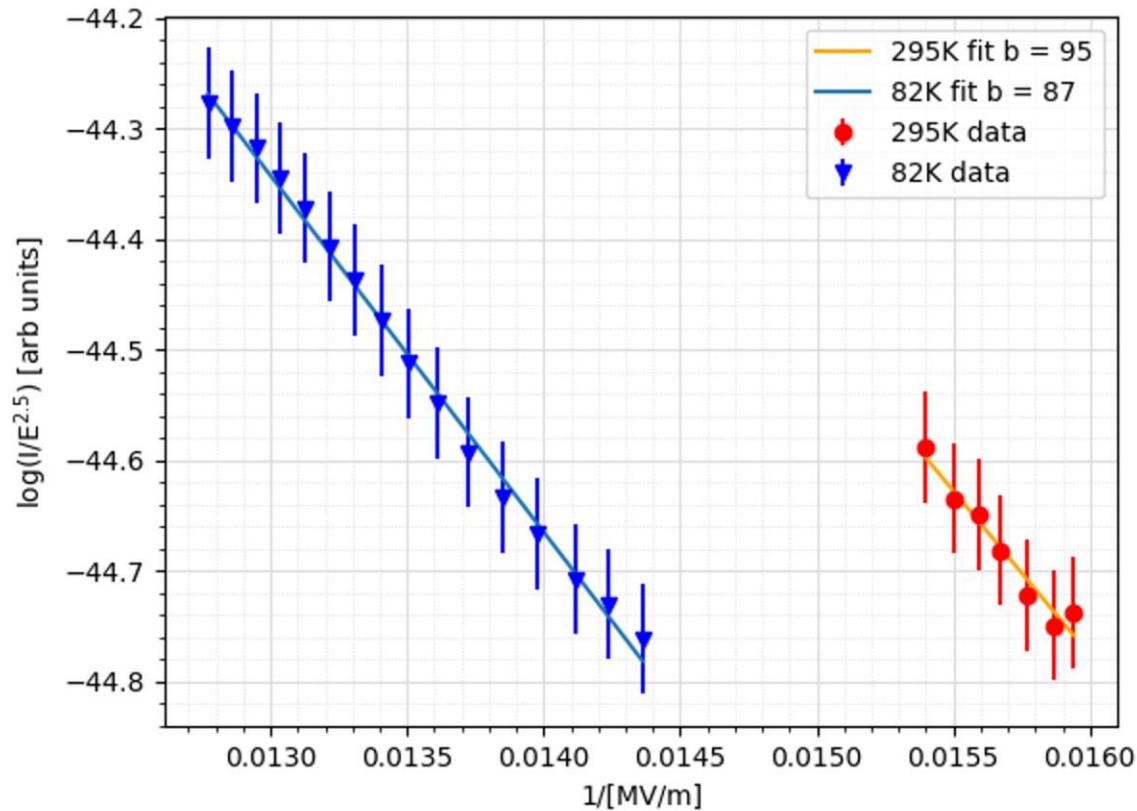




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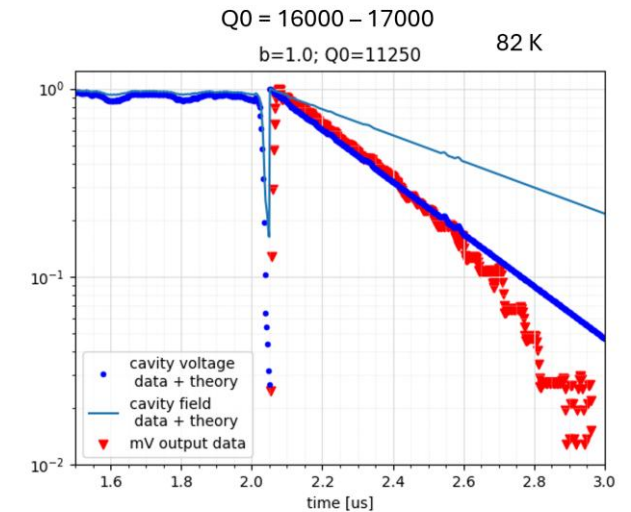
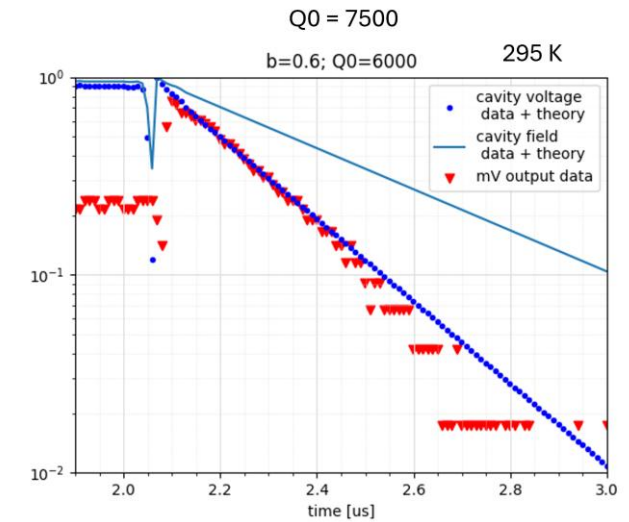
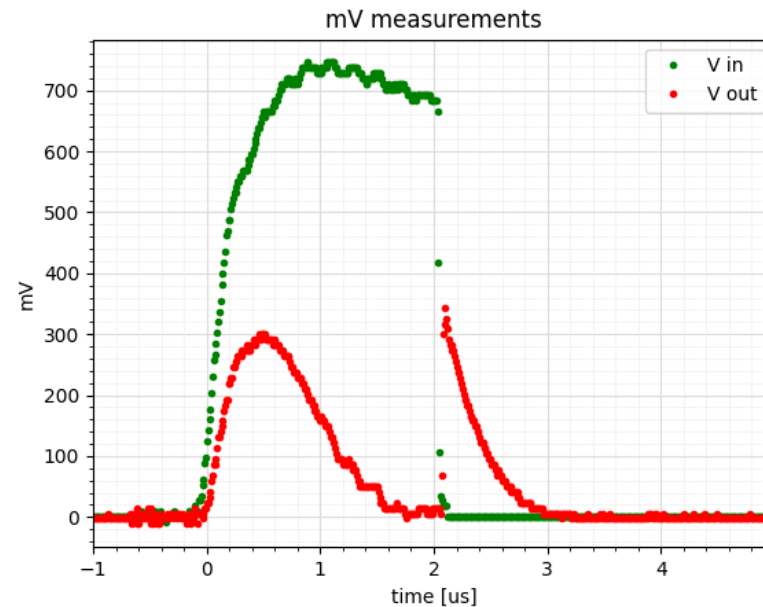


# Cryogenic Dark Current



- Approximate total charge can be estimated via *beam loading* i.e. measured loss in  $Q_0$  from expected values in presence of excess charge giving approx. 10s pC
- From additional PIC simulation analysis, 7-8% of electrons make it >30 cm downstream, so < 1 pC expected downstream (25+ cm)
- 10-100 pC/2  $\mu$ s = 5-50  $\mu$ A total and 0.5 pC expected downstream
- 500  $\mu$ A in LCLS, 50  $\mu$ A in SwissFEL, 10  $\mu$ A in superconducting EuXFEL (2 m downstream)

G. Shu et al, *Nuclear Instruments and Methods in Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment*, Volume 1010, 2021, 165546, ISSN 0168-9002, doi:10.1016/j.nima.2021.165546.





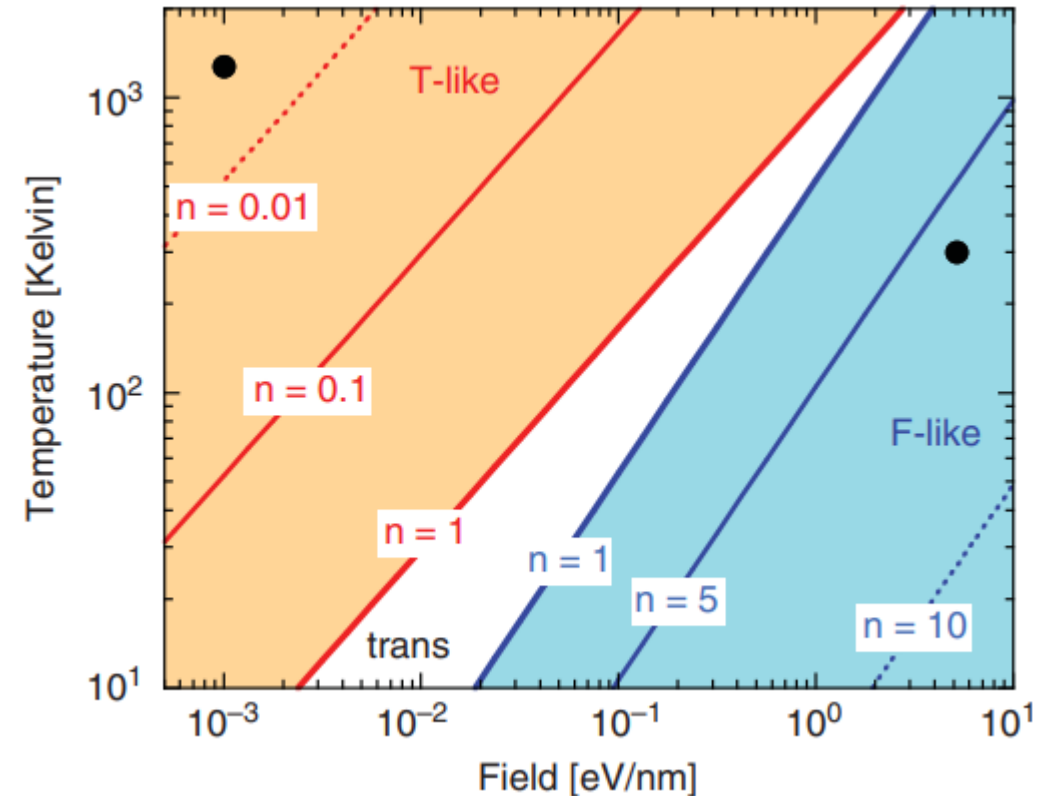
# GTF emission



- Rather than Fowler –Nordheim for completeness use a general thermal-field emission model via Jensen that incorporates thermionic and field emission contributions

$$J_{GTF}(F, T) = \begin{cases} n^{-2} J_F + J_T & (n < 1) \\ J_F + n^2 J_T & (n > 1) \end{cases}$$

Jensen, Kevin L., and Marc Cahay. "General thermal-field emission equation." *Applied physics letters* 88.15 (2006).



Jensen, Kevin L. *Introduction to the physics of electron emission*. John Wiley & Sons, 2017.



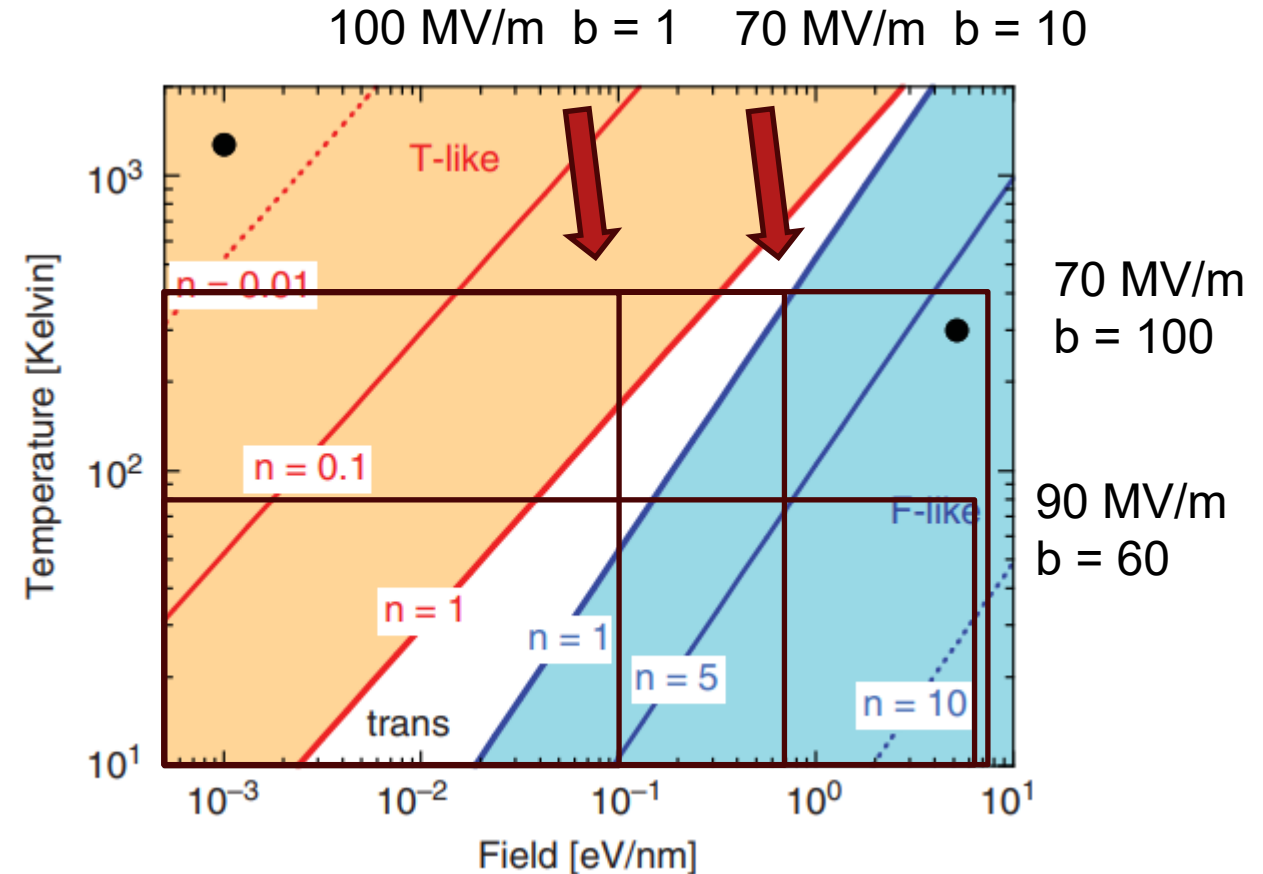
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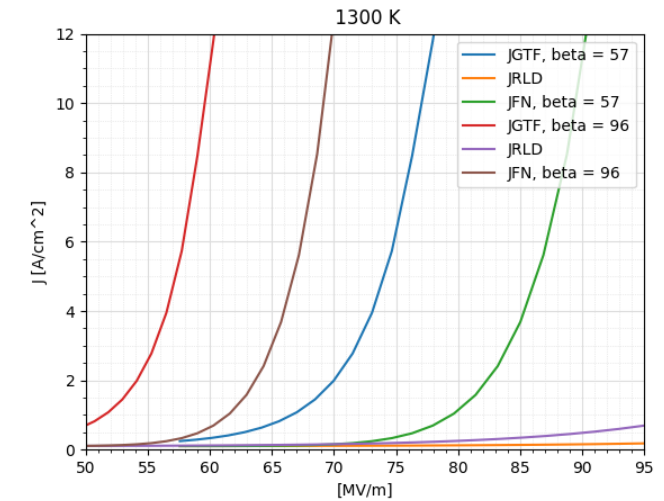
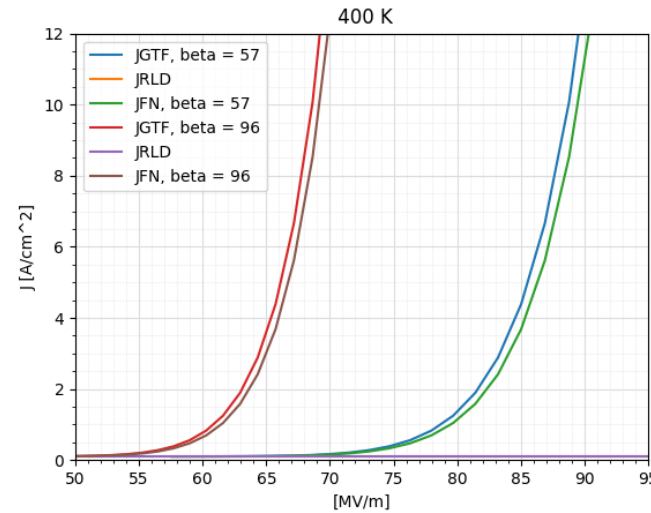
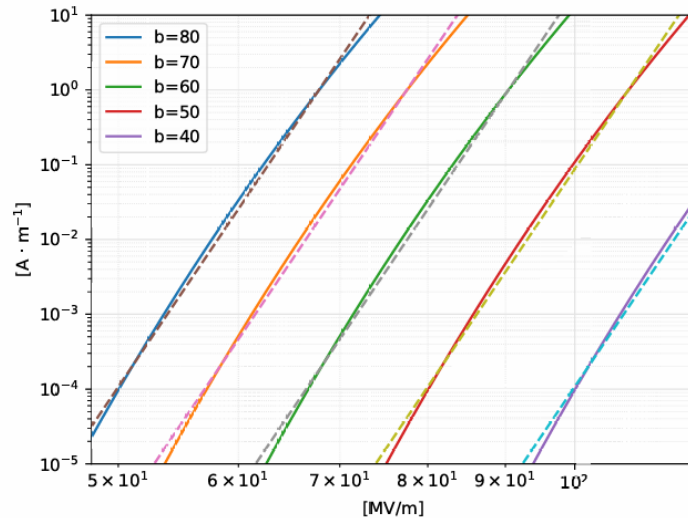
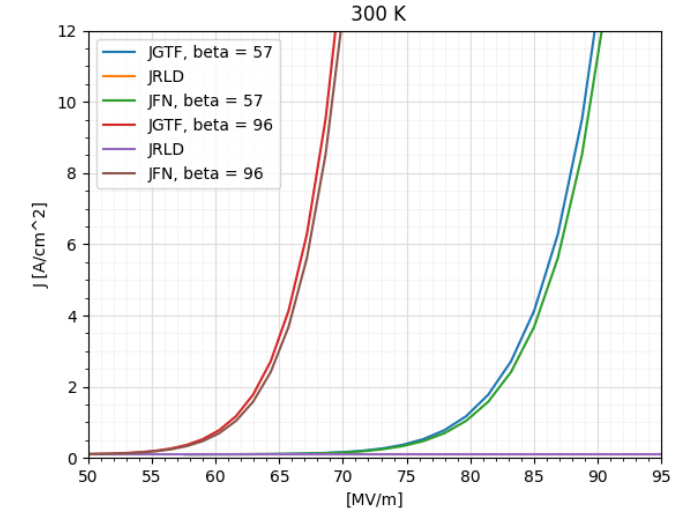
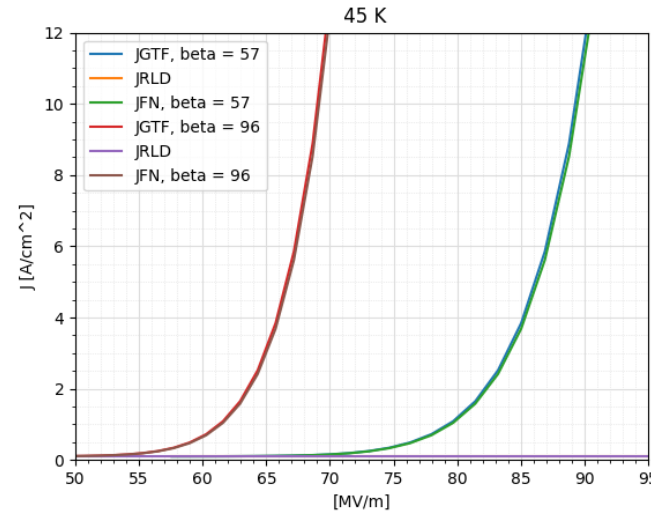
Jensen, Kevin L. *Introduction to the physics of electron emission*. John Wiley & Sons, 2017.



# GTF emission



- Pulse heating needed to achieve some reasonable visible effect (400 K)
- But Cu melts at certain temperatures
- Scaling similar to BDR in high gradient regime,  $E^{30}$  (below)



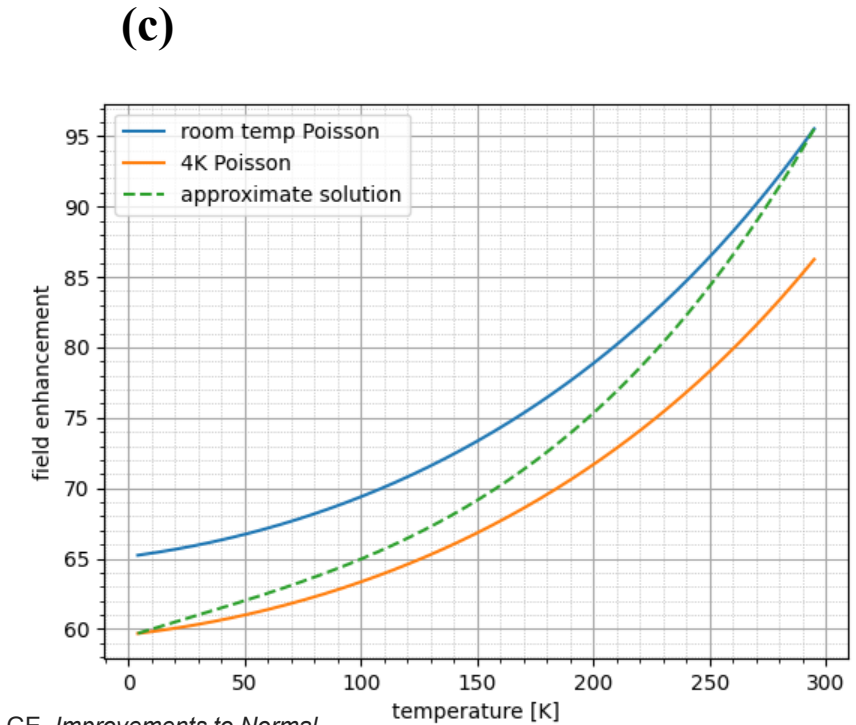
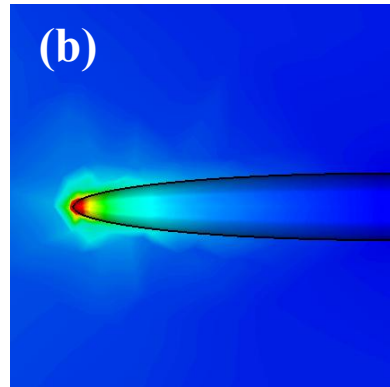
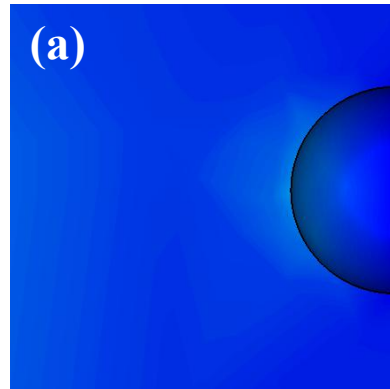
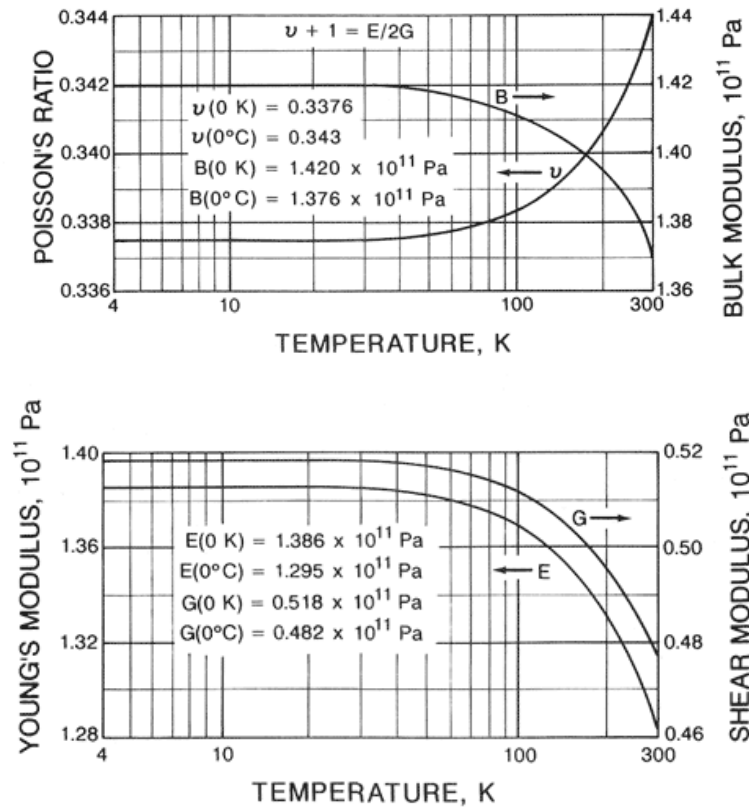




# Emission tip model



- Temperature dependence not present in Fowler-Nordheim tunneling
- Useful simple model, taking effective  $\beta$ , and scaling field to get geometric deformation empirically to obtain room temperature value
- Then using NIST Young's modulus and Poisson ratio for copper to obtain reduced field enhancement geometry at low temperatures due to increased material hardness



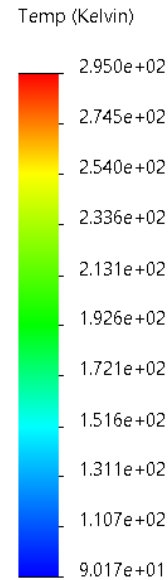
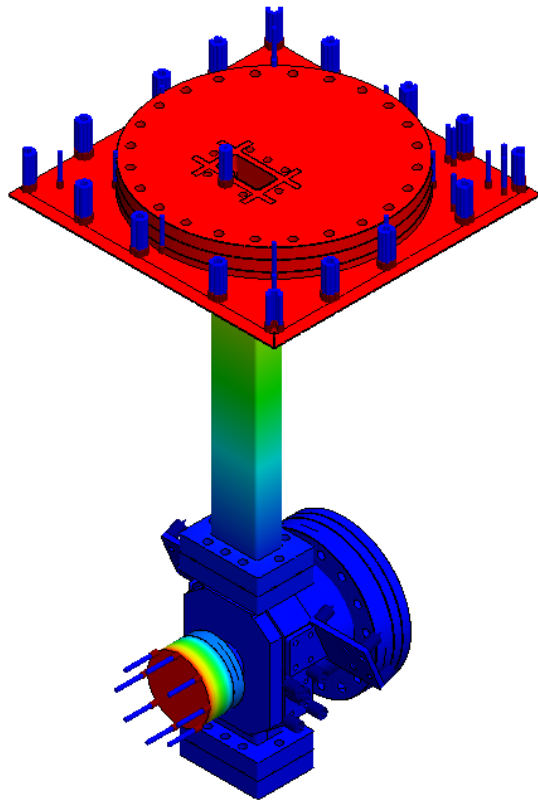
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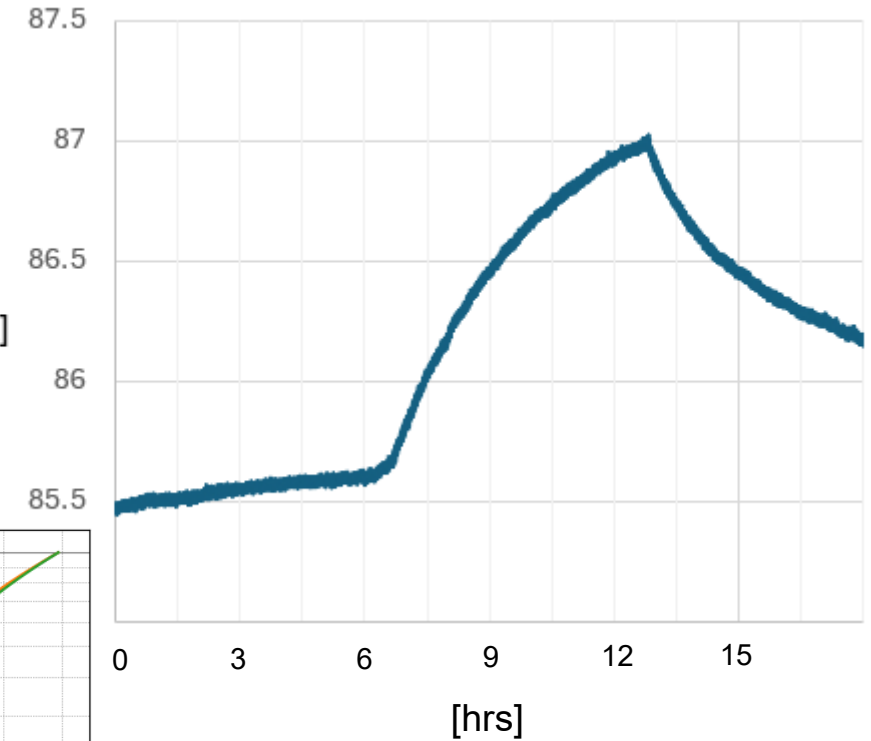
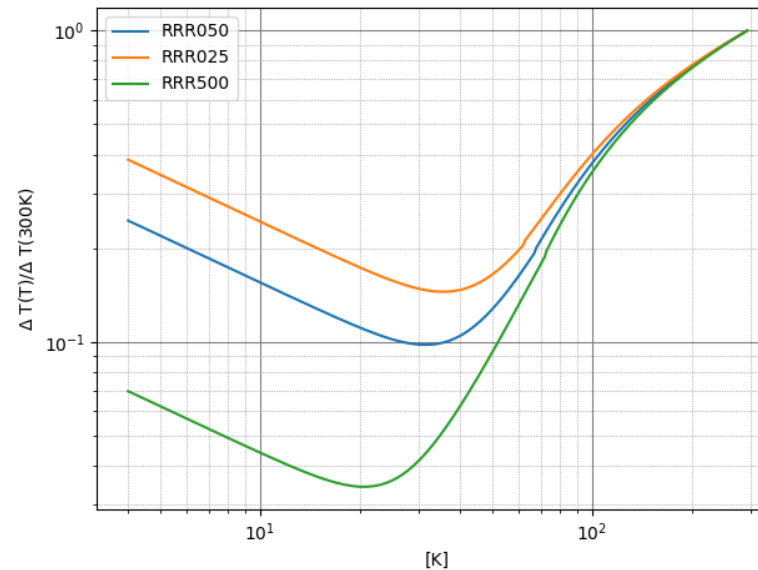
# RF heating contribution



- Main gun section shown outside of cryostat (far left)
- Simplified thermal steady state simulation shown (middle) with previous cooling configuration to show accuracy of transient cooling simulations given estimated heat leaks from waveguide, beam pipe etc.
- RF heating over 6 hours (right) at 1 Hz  $\approx 0.8$  W



$$\Delta T(T) = \frac{R_s(T) |H_{||}|^2 \sqrt{t}}{\sqrt{\pi \rho' c_e \sigma L T}} \propto \frac{R_s(T)}{\sqrt{\rho' c_e \sigma L T}} \propto \frac{R_s(T)}{\sqrt{\rho' c_e \sigma T}} \quad [\text{K}]$$

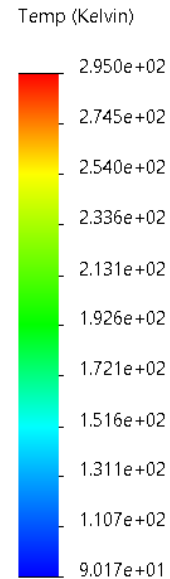
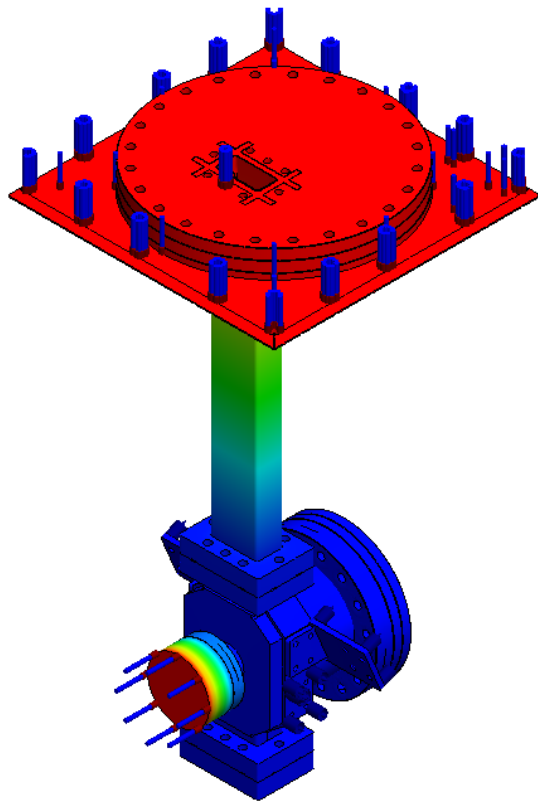




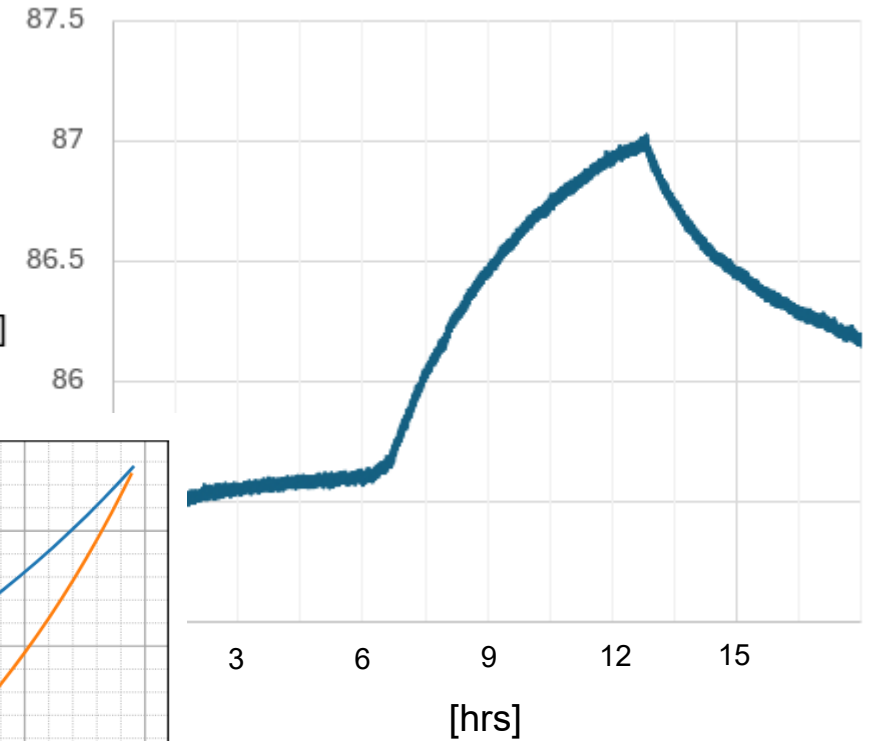
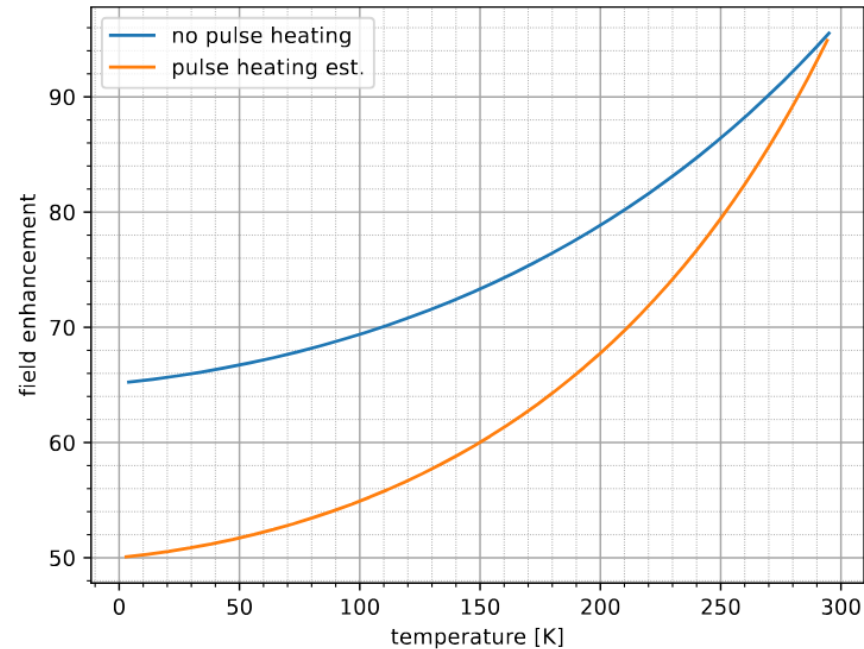
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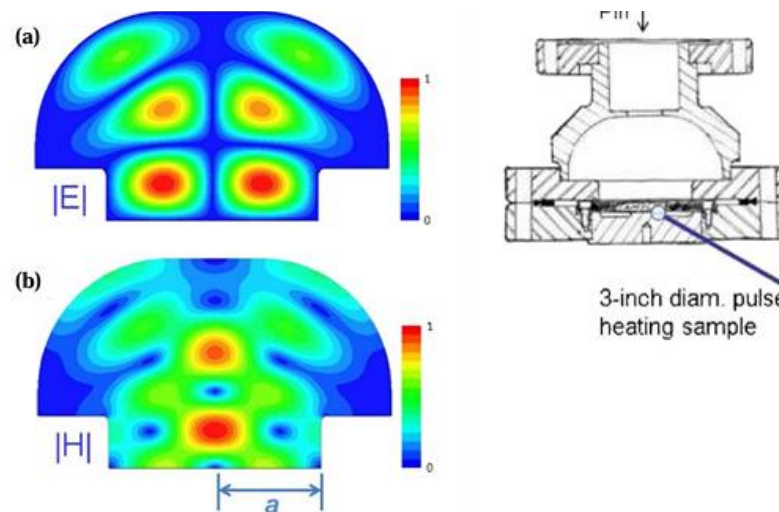
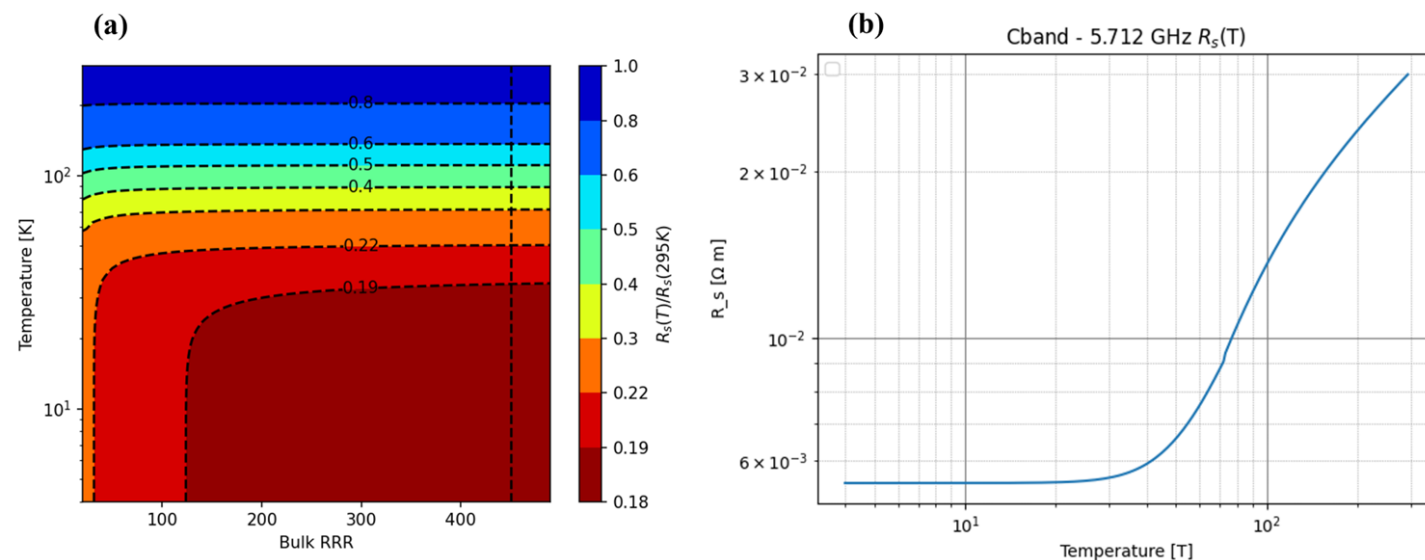
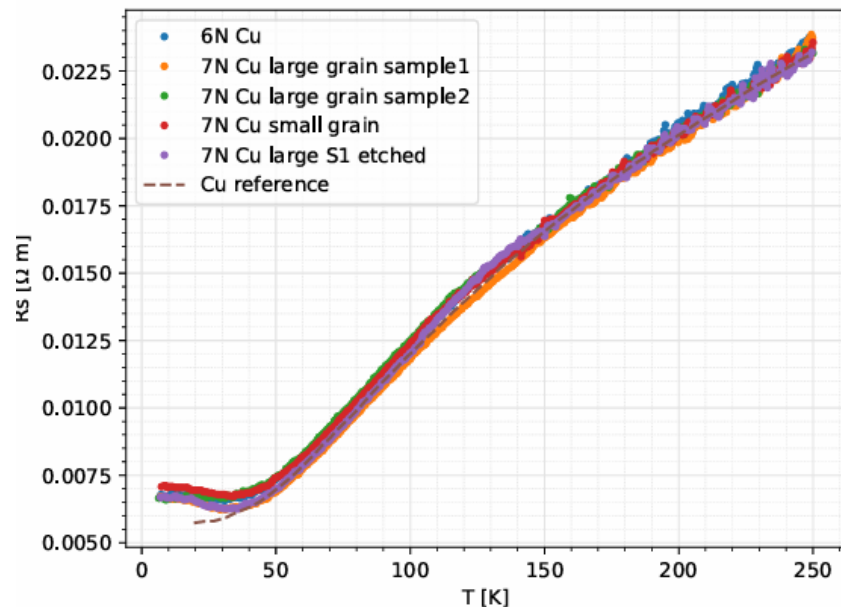




# Temperature dependent RF resistance



- Surface resistance minimum at cryogenic temperatures measured for samples in SLAC mushroom dome cavity
- Plotted for various RRR (right)



Laurent, Lisa, et al. "Experimental study of rf pulsed heating." *Physical Review Special Topics—Accelerators and Beams* 14.4 (2011): 041001.

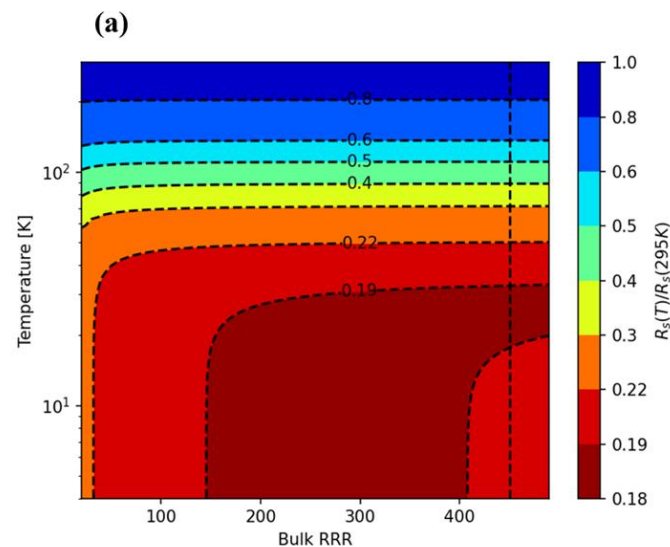
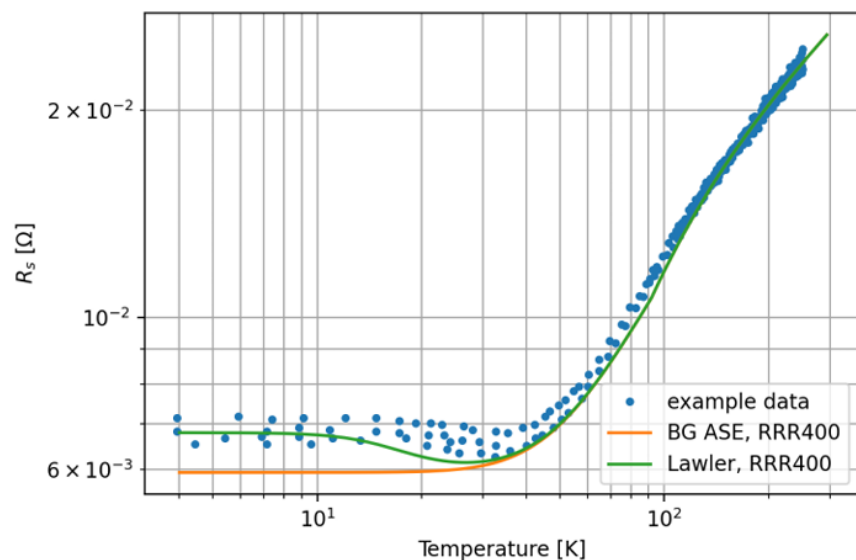


# Thin film model

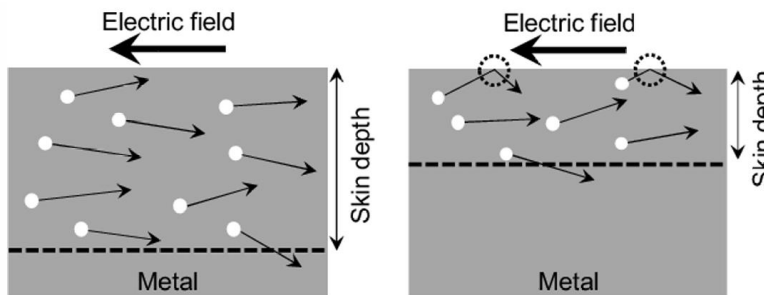


- Thin film explanation via theory of Gurzhi which found local minimum in surface resistance at cryo

R. Gurzhi, "Contribution to the theory of the skin effect in metals at low temperatures," Sov. Phys. JETP, vol. 20, pp. 1228–1230, 1964.

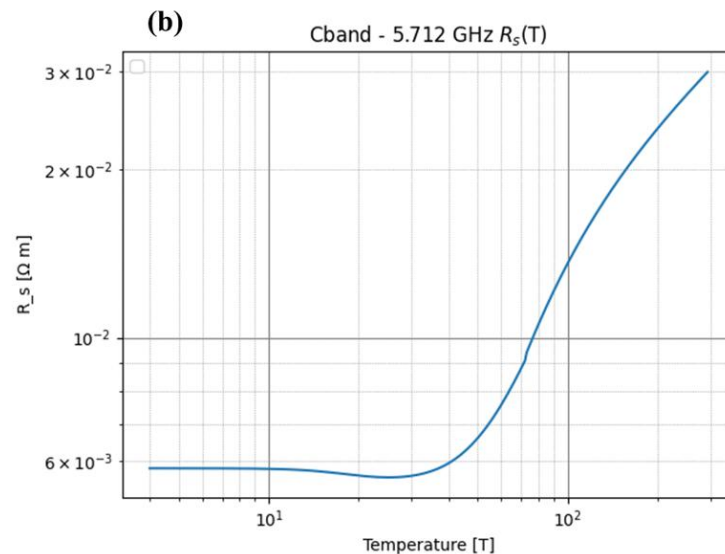


Lawler, Gerard, Fabio Bosco, and James Rosenzweig. "Improving interface physics understanding in high-frequency cryogenic normal conducting cavities." *arXiv preprint arXiv:2310.11578* (2023).

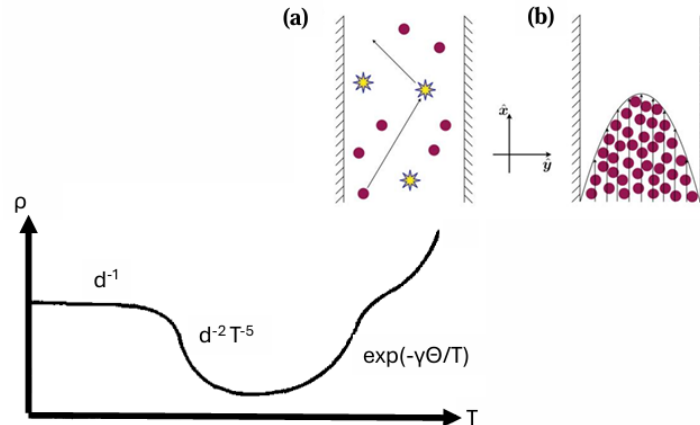


(a)

(b)



Polini, Marco, and Andre K. Geim. "Viscous electron fluids." *Physics Today* 73.6 (2020): 28-34.



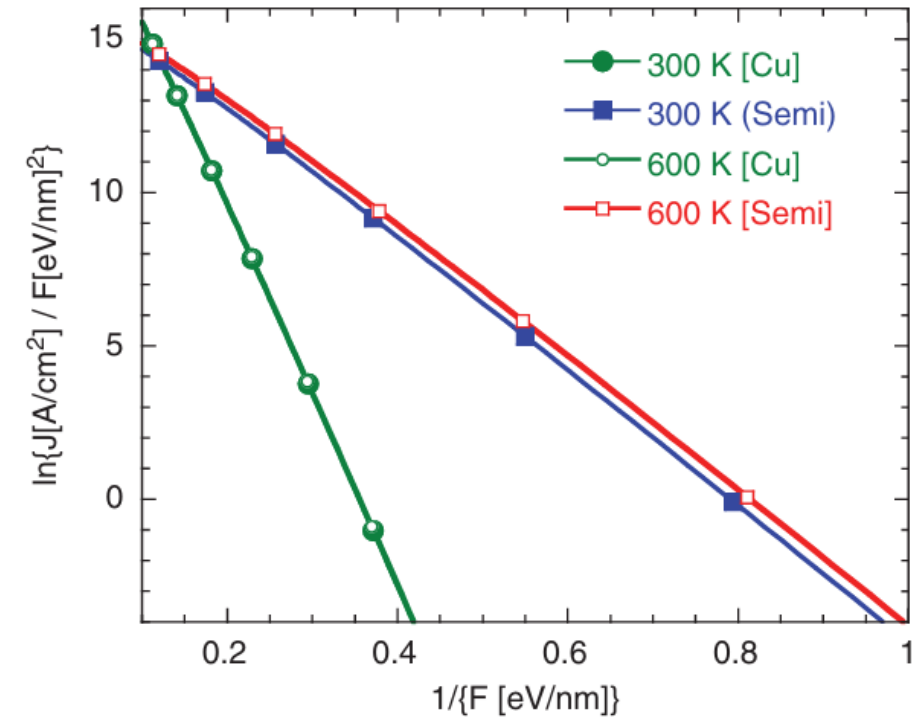
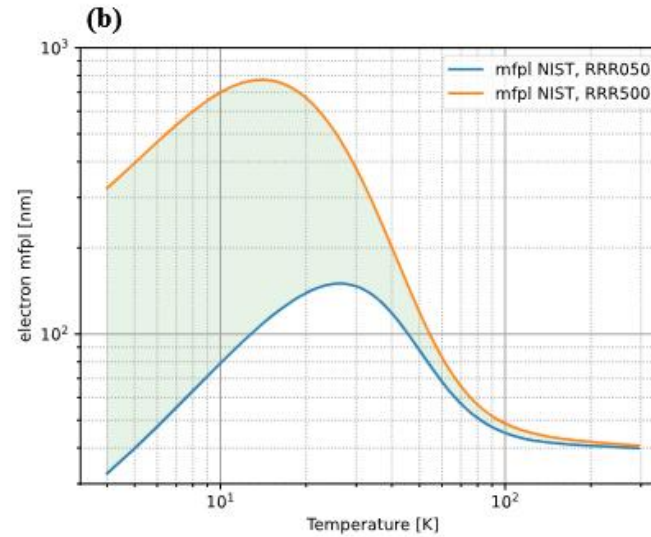
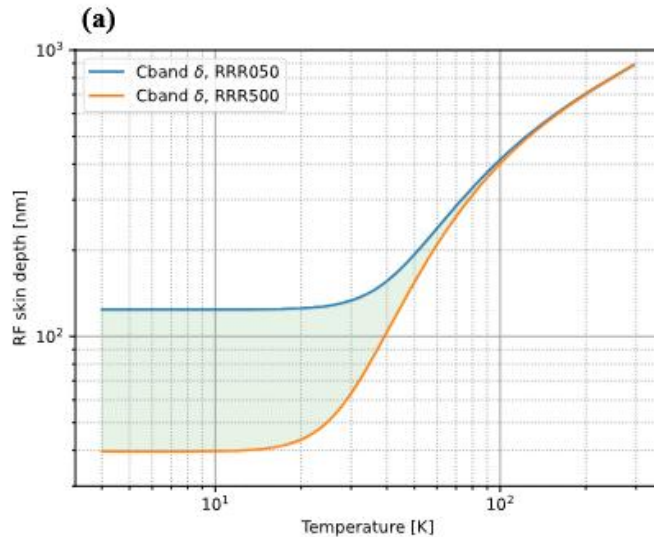




# Thin film implications



- in ASE regime for Cband for examples drops into 10s nm
- Thin film behavior may lead to more semiconductor like behavior leading to temperature changes have a greater consequence
- Field emitted current as function of inverse field example (right) from Jensen demonstrating qualitatively reduced value as temperature goes down
- Cryogenic temperature extension needed



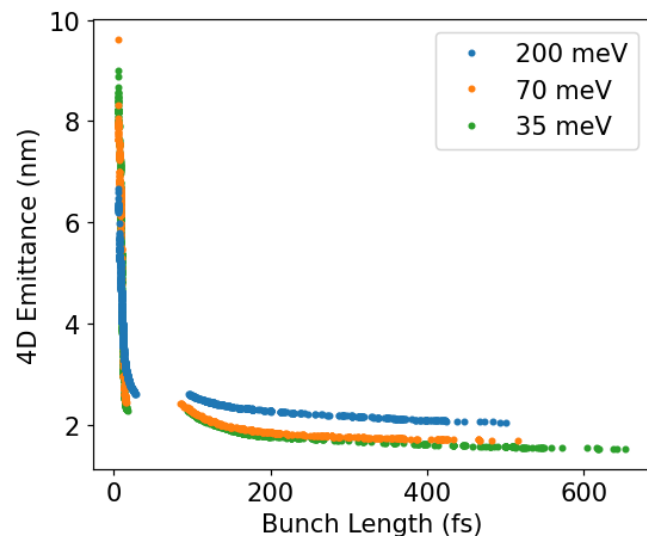
Jensen, Kevin L. *Introduction to the physics of electron emission*. John Wiley & Sons, 2017.



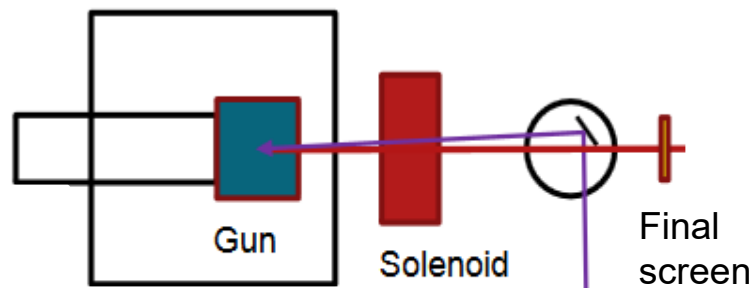
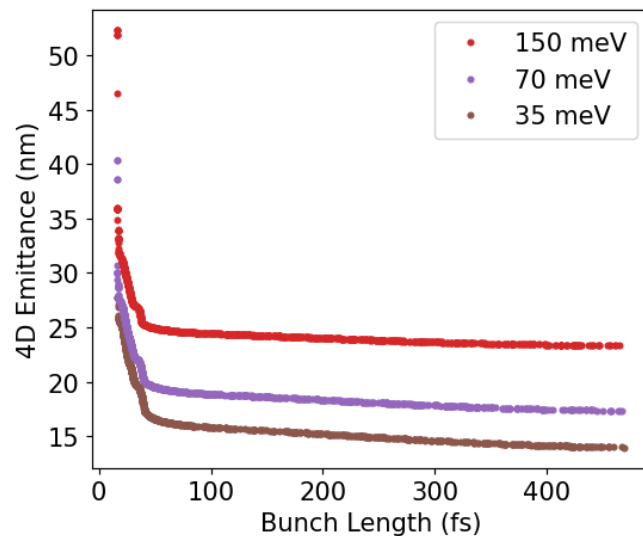
# Multiobjective optimizations for UED



(a)



(b)



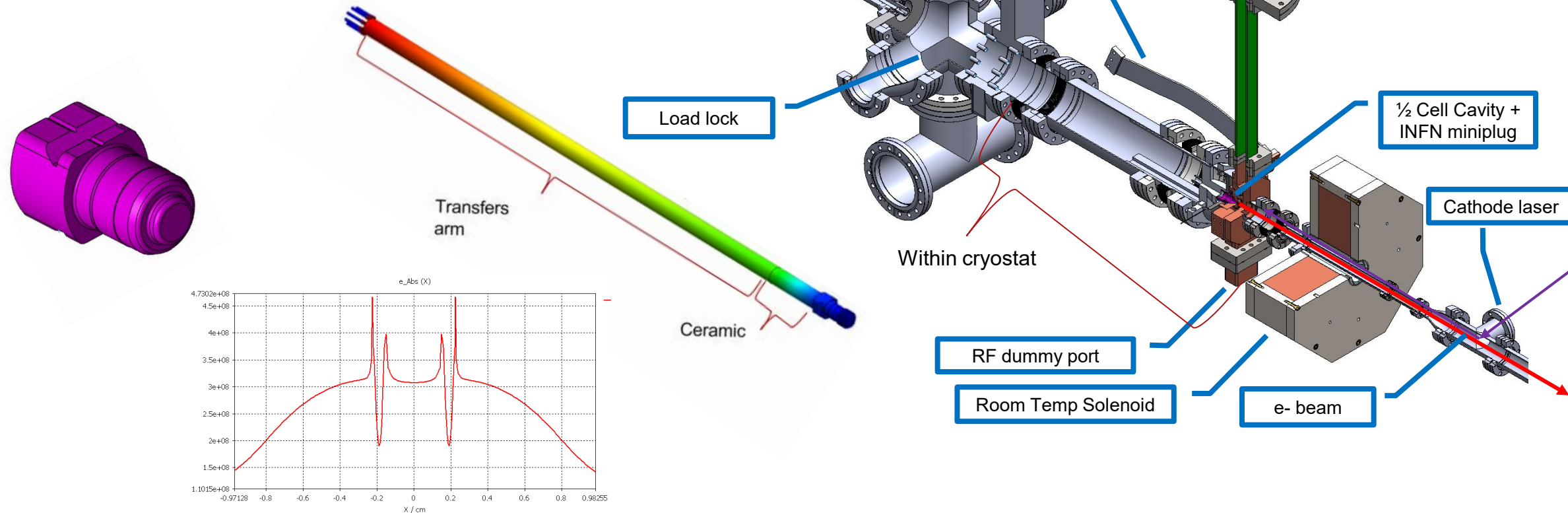
Variables	Range
Gun phase offset ( $\Delta\phi$ )	$[-10, 10]$ degrees ( $\phi_0 = 125$ deg)
Solenoid position	$[0.24, 0.6]$ m
Sol strength	$[0.0, 3.0]$ (0.95-> ~0.13 T)
Initial bunch length	$[50, 300]$ fs

Constants	Value
Charge	16 fC
Peak field	180 MV/m
Screen (sample)	1.5 m
Spot size at cathode	(a) $1.2 \mu\text{m}$ (b) $40.0 \mu\text{m}$



# Phase2 Load lock

- Difficulty of interference fit for cathode coupling not reliable in near term
- Shift to knife edge coupling with sufficiently thermally isolated transfer arm





# 5. Conclusions



1. High gradient cavities here means BDR reduced meaning cryogenic and/or heating minimized leads to increasing consideration of dark current needed
2. Empirical cryogenic reduction could be advantageous for high gradient brightness operation complementary to BDR reduction alone
3. Physics of emission at cryogenic temperatures complex and interesting
4. Capabilities to study increasing significantly at UCLA and LANL



# 5. Conclusions



- Fabio Bosco, Obed Camacho, Atsushi Fukasawa, David Garcia, *Richard Li*, Pietro Musumeci, Brian Naranjo, Pratik Manwani, Jake Parsons, *April Smith*, *Sean O'Tool*, Yusuke Sakai, Oliver Williams, Monika Yadav



- Paul Carriere, Nanda Matavalam



- Evgenya Simakov, Anna Alexander, Petr Anisimov, Haoran Xu



- Martina Carillo, Andrea Mostacci



- Zenghai Li, Sami Tantawi, Nathan Majernik



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- Chad Pennington, Jared Maxxson