

Thermal Modeling and Benchmarking of Crystalline Laser Amplifiers

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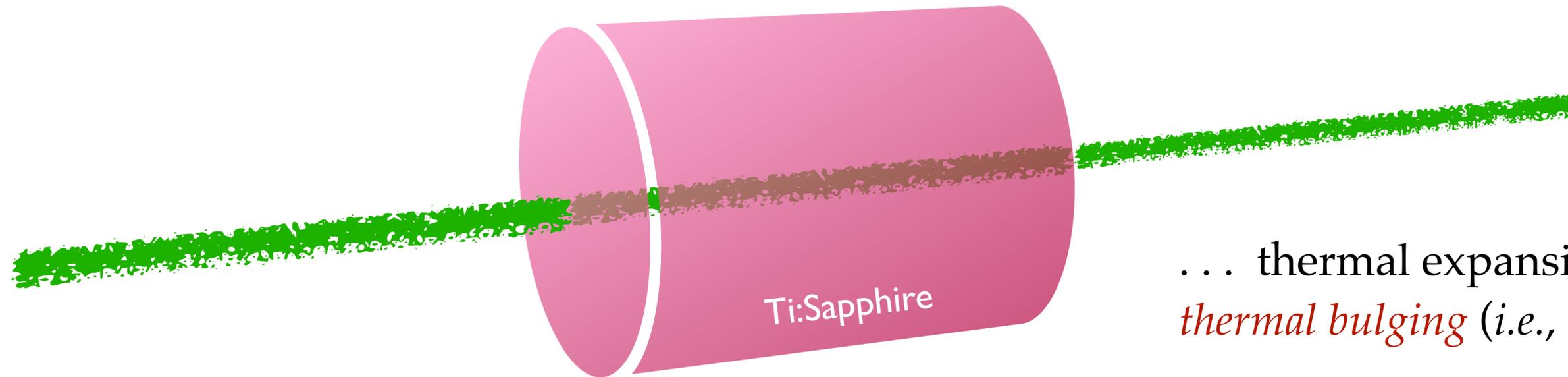


Motivation: Why Model Thermal Effects in Crystalline Laser Amplifiers?

At high power and high intensity, thermal gradients induce ...

... positional variation of the refractive index, hence *thermal lensing*

... , with direction-dependent thermal conductivity, hence *astigmatism*



... thermal expansion, hence *thermal bulging* (i.e., more lensing)

... mechanical stresses, hence *modified birefringence*

Conservation of Energy and Fourier Heat Law yield (Nonlinear) Heat Equation

conservation of energy: $\rho \dot{u} = -\nabla \cdot \vec{q} + \dot{\epsilon}(\vec{r}, t)$

ρ : mass density
 \dot{u} : internal energy per unit mass
 \vec{q} : heat flux
 $\dot{\epsilon}(\vec{r}, t)$: source term

Fourier law: $\vec{q} = -\kappa \nabla \theta$

κ : thermal conductivity
 θ : temperature

specific heat capacity: $c_p = \frac{\partial u}{\partial \theta}$

relates gradients of energy and temperature: $\nabla u = \frac{\partial u}{\partial \theta} \nabla \theta = c_p(\theta) \nabla \theta \implies \vec{q} = -\frac{\kappa(\theta)}{c_p(\theta)} \nabla u$

(nonlinear) heat equation: $\dot{u} = -\frac{1}{\rho} \nabla \cdot \vec{q} + \frac{1}{\rho} \dot{\epsilon}(\vec{r}, t) = \nabla \cdot \left(\underbrace{\frac{\kappa(\theta)}{\rho(\theta) c_p(\theta)}}_{\alpha(\theta)} \nabla u \right) + \frac{\kappa}{(\rho c_p)^2} \frac{\partial \rho}{\partial \theta} |\nabla u|^2 + \frac{1}{\rho} \dot{\epsilon}(\vec{r}, t)$

linear heat equation:

$$\dot{u} = \alpha \nabla^2 u + \frac{1}{\rho} \dot{\epsilon}(\vec{r}, t)$$

$\alpha(\theta) \rightarrow \alpha(u)$
 thermal diffusivity

neglect this term if density has a very weak dependence on temperature

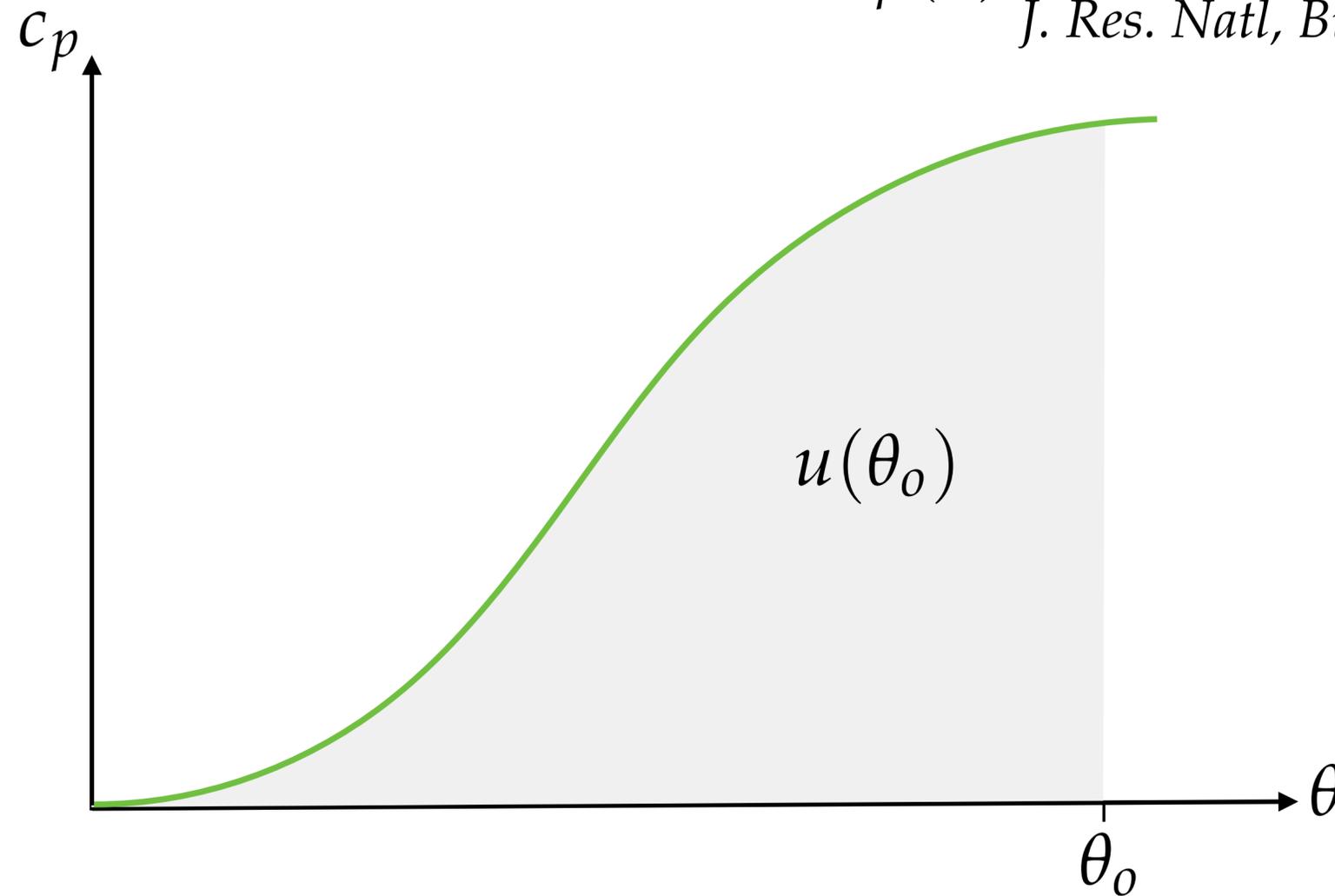
Specific Heat Capacity Connects Internal Energy and Temperature

specific heat capacity: $c_p = \frac{\partial u}{\partial \theta}$

$\kappa(\theta)$ ER Dobrovinskaya, LA Lytvynov, and V Pishchik, "Properties of Sapphire", in *Sapphire: Material, Manufacturing, Applications*, (Springer, Boston, MA) 55–176, January 2009.

DOI: 10.1007/978-0-387-85695-7_2

$c_p(\theta)$ DA Ditmars, S Ishihara, SS Chang, G Bernstein, and ED West, *J. Res. Natl. Bur. Std.* 87(2):159–163, March-April 1982.



$$\kappa(\theta) \rightarrow \kappa(u)$$

$$c_p(\theta) \rightarrow c_p(u)$$

$$\frac{\kappa(\theta)}{\rho(\theta)c_p(\theta)} \rightarrow \alpha(u)$$

NB: Sapphire \neq Ti:Sapphire

Our Present Focus: Thermal Equilibrium with a Gaussian Pump Source

Time Scales for Thermal Relaxation (*linear* heat equation)

Fourier-Bessel series expansion

$$\Theta(r, z; t) = \sum_{n=1}^{\infty} \sum_{m=0}^{\infty} \Theta_{nm} J_0\left(\frac{\nu_{0n} r}{a}\right) \cos\left(\frac{m\pi z}{l}\right) e^{-t/\tau_{nm}}$$

$$\tau_{nm}^{-1} = \alpha \left[\left(\frac{\nu_{0n}}{a}\right)^2 + \left(\frac{m\pi}{l}\right)^2 \right] \quad \text{dominant time-scale: } \tau_{10} = \frac{a^2}{\nu_{01}^2 \alpha}$$

Power Deposition and Equilibrium Temperature (*linear* heat equation)

transverse gaussian
× longitudinal decay

$$g(r, z) = g_0 g_{\perp}(r) g_{\parallel}(z) = g_0 e^{-(r/\sigma)^2} e^{-z/\zeta} \leftarrow \dot{\epsilon}(\vec{r}, t)$$

$$\Theta(r, z) = \Theta_0 \sum_{n=1}^{\infty} \sum_{m=0}^{\infty} (X_{nm} R_n Z_m) J_0\left(\frac{\nu_{0n} r}{a}\right) \cos\left(\frac{m\pi z}{l}\right) \quad \Theta_0 = \frac{P_{\text{abs}}}{4\pi K_c} \frac{V_{\text{cyl}}}{V_{\text{eff}}}$$

$$V_{\text{eff}} = \int e^{-(r/\sigma)^2} e^{-z/\zeta} d^3\vec{r} = \pi\sigma^2\zeta(1 - e^{-l/\zeta})$$

$$R_n = \frac{2}{[\nu_{0n} J_1(\nu_{0n})]^2} \int_0^{\nu_{0n}} x \exp\left[-\left(\frac{ax}{\nu_{0n}\sigma}\right)^2\right] J_0(x) dx \quad Z_m = \frac{2}{1 + \delta_{m0}} \frac{l/\zeta}{(l/\zeta)^2 + (m\pi)^2} [1 - (-1)^m e^{-l/\zeta}]$$

“cross”-term (from solving heat equation with vanishing time dependence) $\rightarrow X_{nm} = \frac{l/a}{(\nu_{0n}l/a)^2 + (m\pi)^2}$

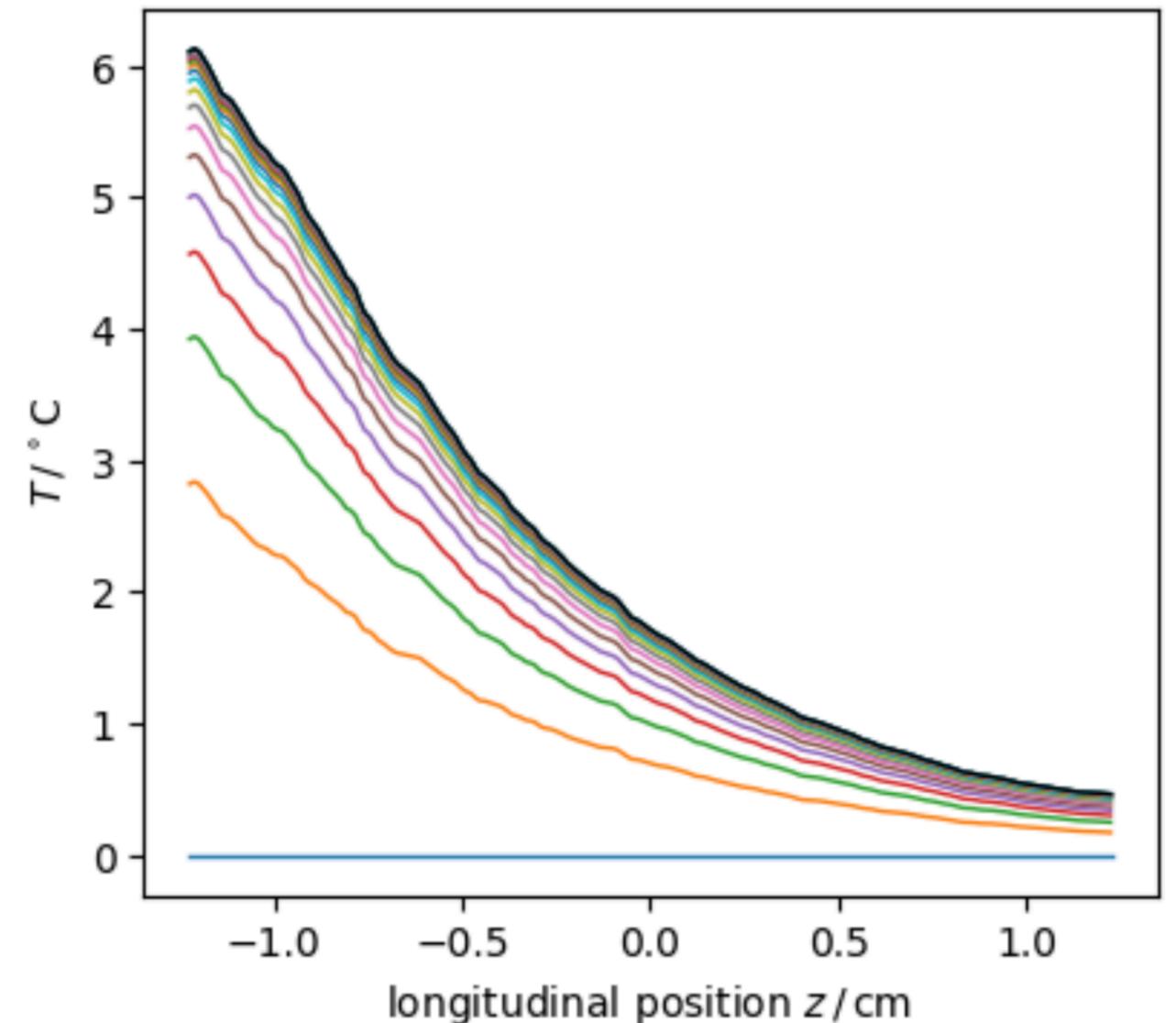
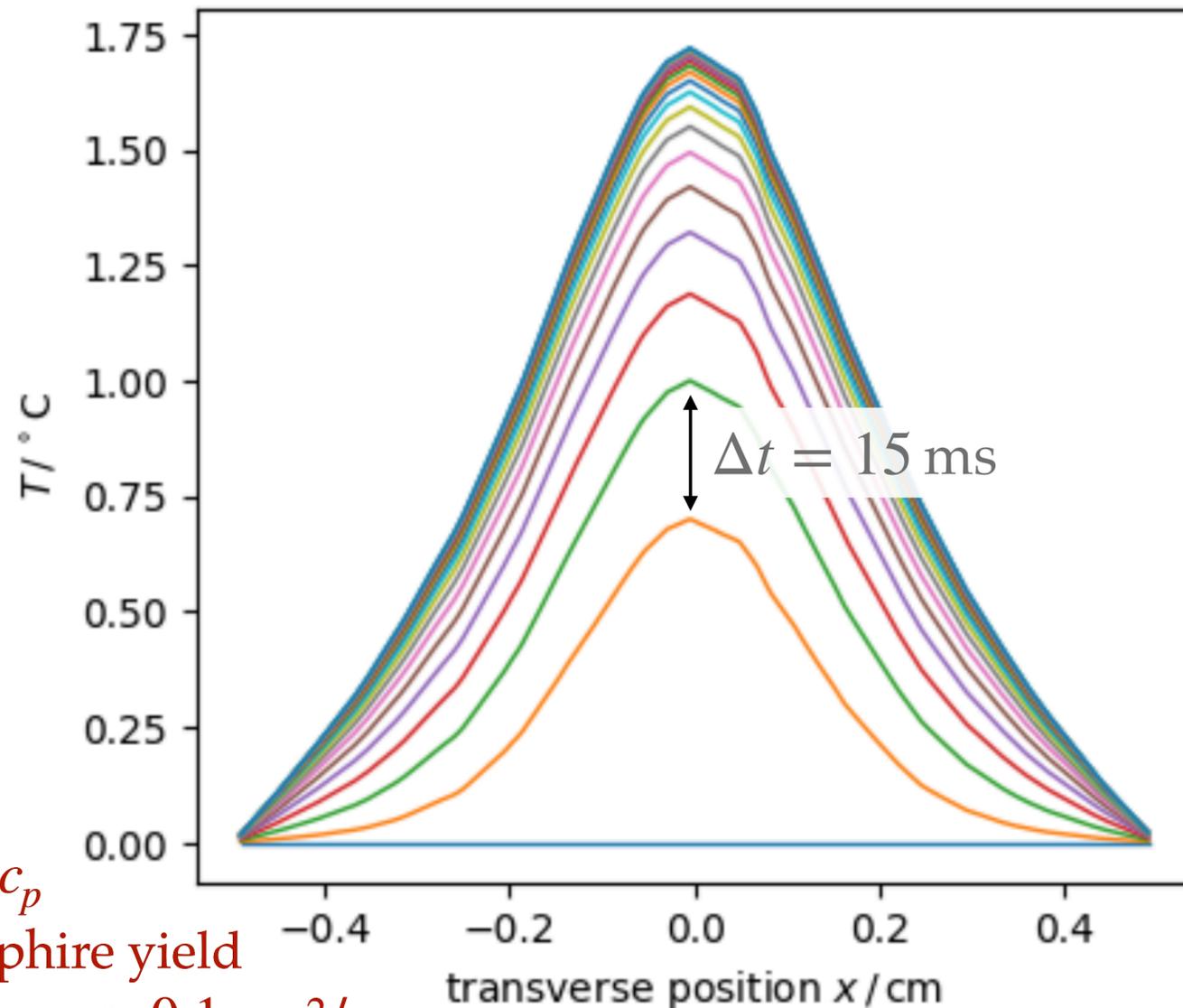
Initial Test with Linear Heat Equation: Quantitative Agreement and a Caveat

Cylindrical crystal:
 radius $a = 1$ cm
 length $\ell = 2.5$ cm
 $\kappa = 0.31$ W/cm·K
 $\rho = 3.98$ gm/cm³
 $c_p = 0.267$ J/gm·K
 $\alpha = 0.292$ cm²/s

$$\tau_{10} = \frac{a^2}{\nu_{01}^2 \alpha}$$

$\tau_{10} \approx 150$ ms \Rightarrow
 $\alpha \approx 0.288$ cm²/s

but values of κ and c_p
 tabulated for Ti:sapphire yield
 much smaller values: $\alpha \approx 0.1$ cm²/s.

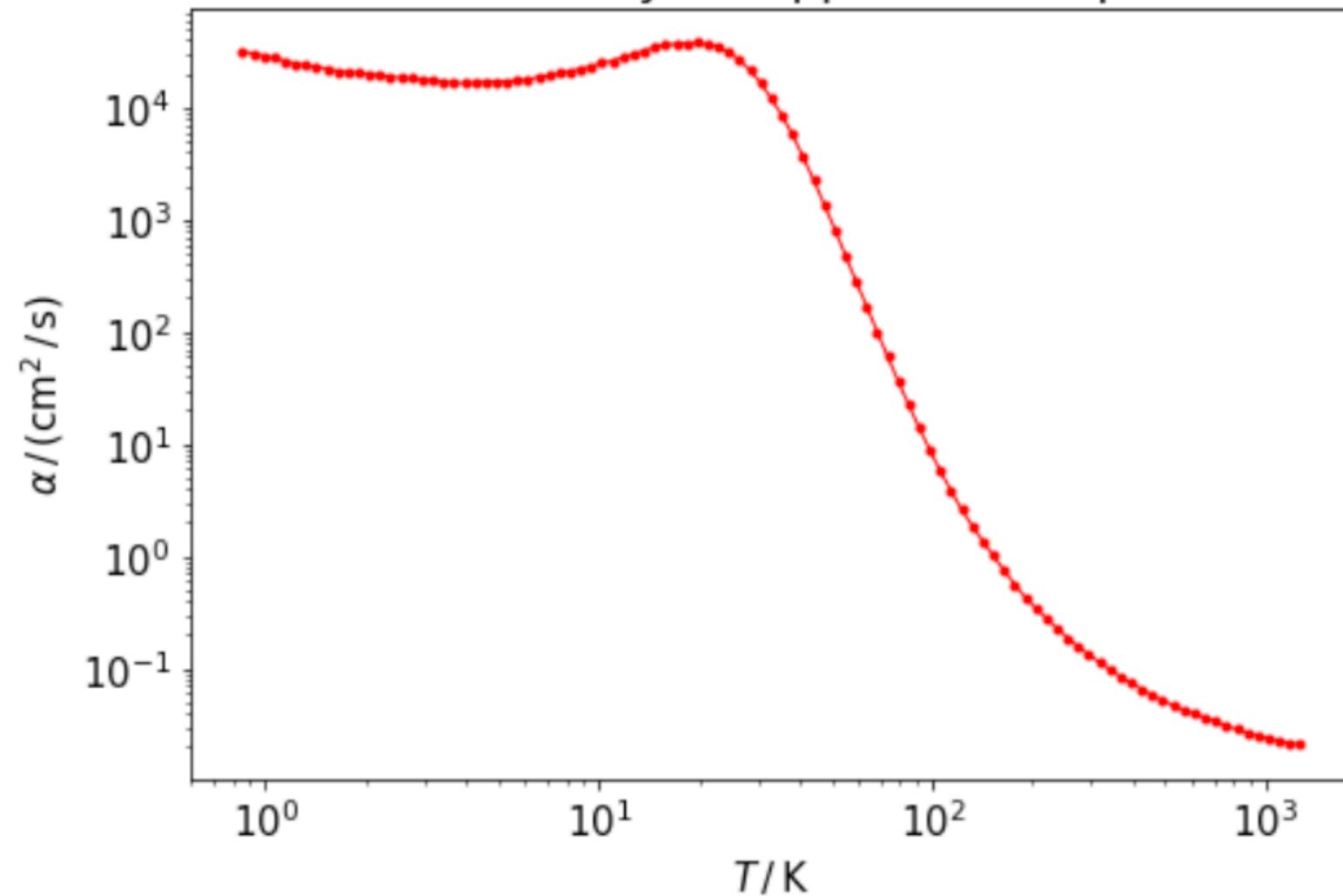


For numerical simulations of general PDEs, we use the open-source *FEniCS Computing Platform* (<https://fenicsproject.org>). It uses UFL, the Unified Form Language (DOI: [10.48550/arXiv.1211.4047](https://doi.org/10.48550/arXiv.1211.4047)), to represent PDEs in variational form. For details of simulation (and theory), see D.T. Abell, *et al.*, in *Proc. IPAC'22*, DOI: [10.18429/JACoW-IPAC2022-THPOTK062](https://doi.org/10.18429/JACoW-IPAC2022-THPOTK062).

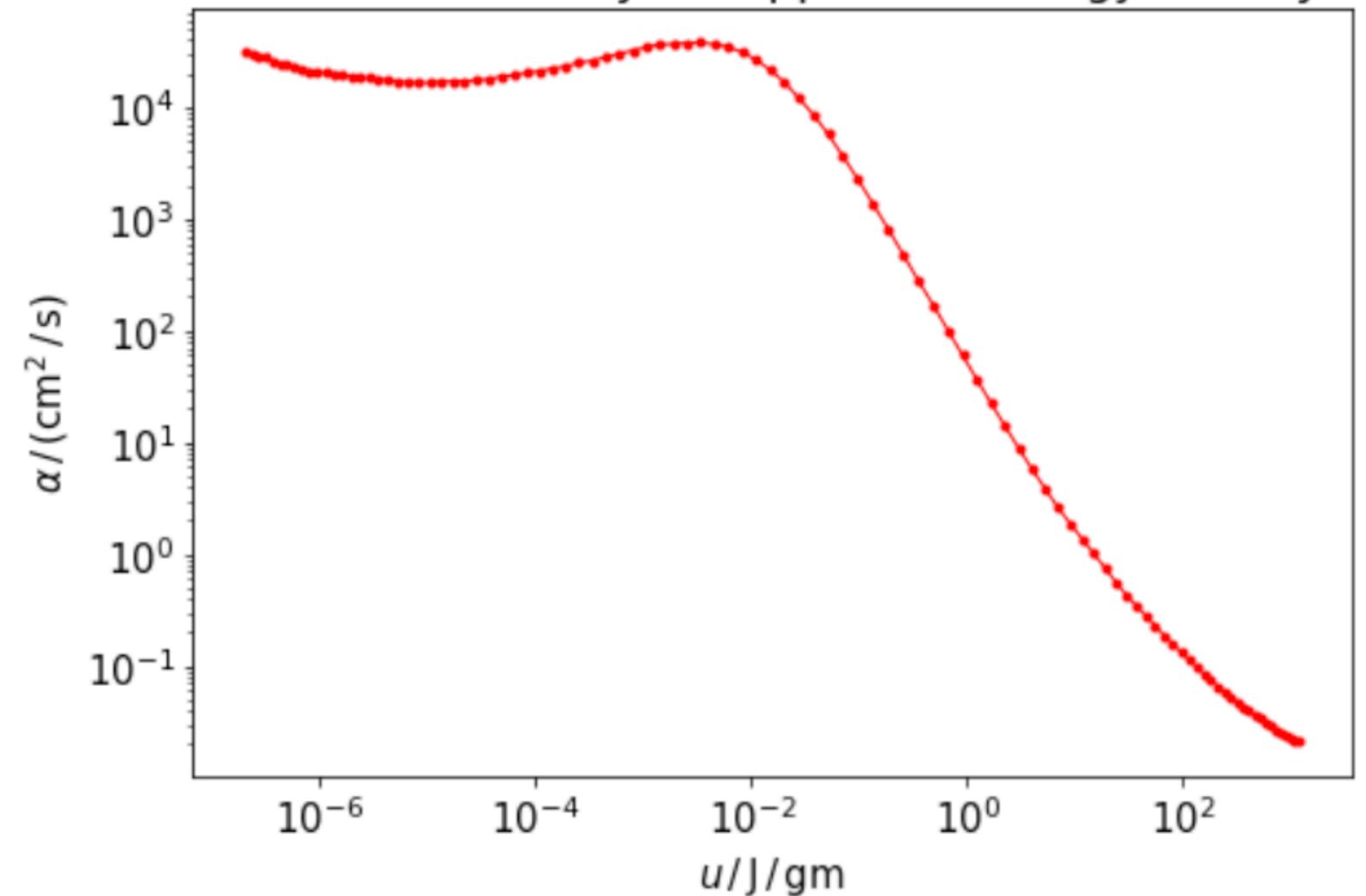
Thermal Diffusivity of Sapphire

On the basis of tabulated and graphical thermodynamic data for sapphire, we constructed the following plots for thermal diffusivity as a function of temperature (left) or internal energy density (right).

thermal diffusivity of sapphire v. temperature



thermal diffusivity of sapphire v. energy density

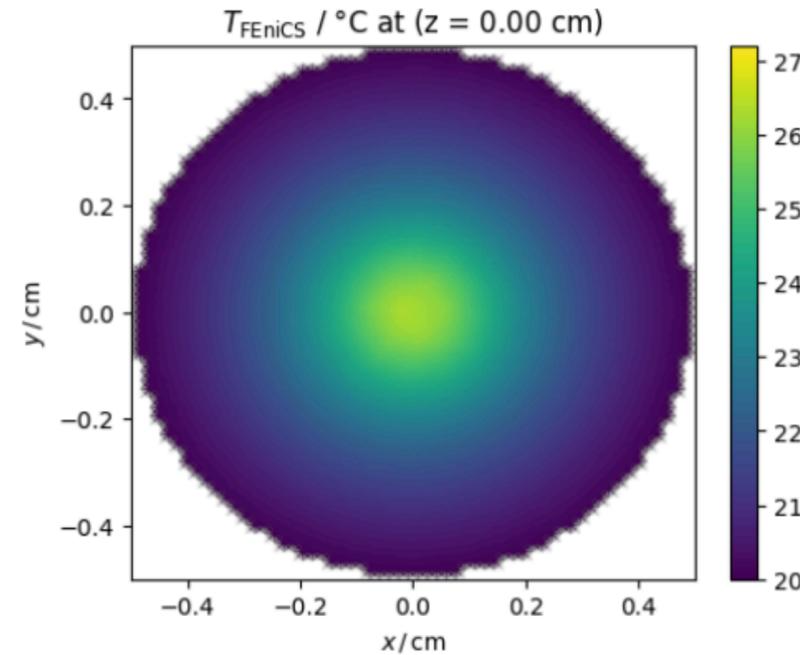


again ... NB: Sapphire \neq Ti:Sapphire

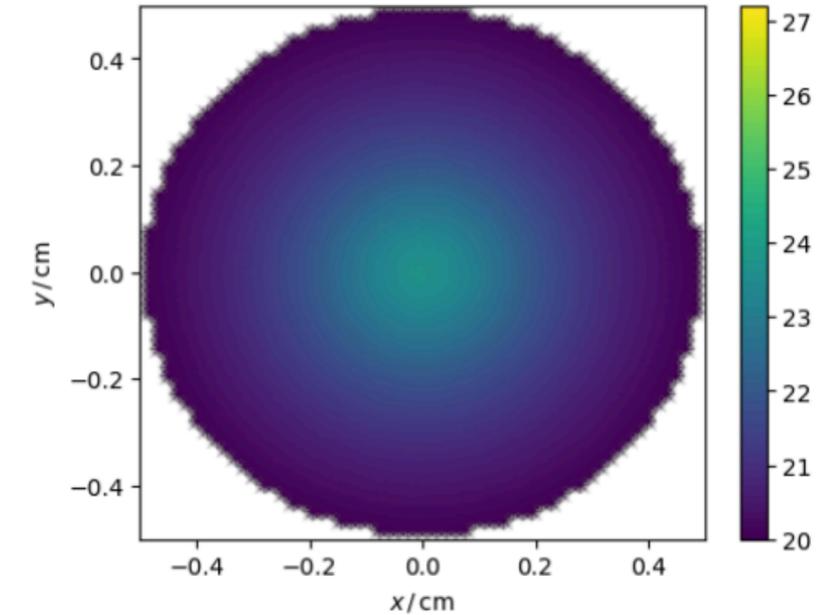
Nonlinear Poisson Equation in Three Dimensions

- Near room temperature, these results appear nearly identical to those of the linear case. (Temperature lineouts appear graphically identical.)
- At an $\times 5$ power level—but still room temperature—we see only mild difference between the linear and nonlinear cases.

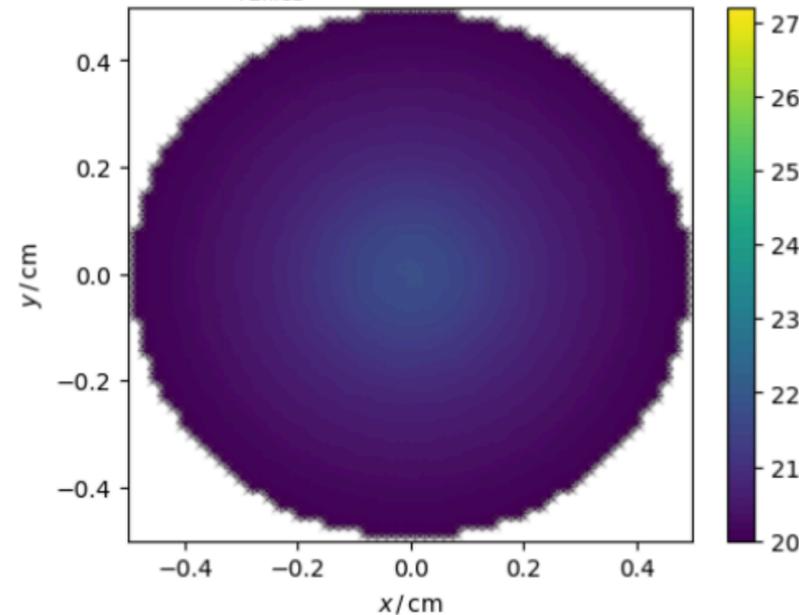
entrance face



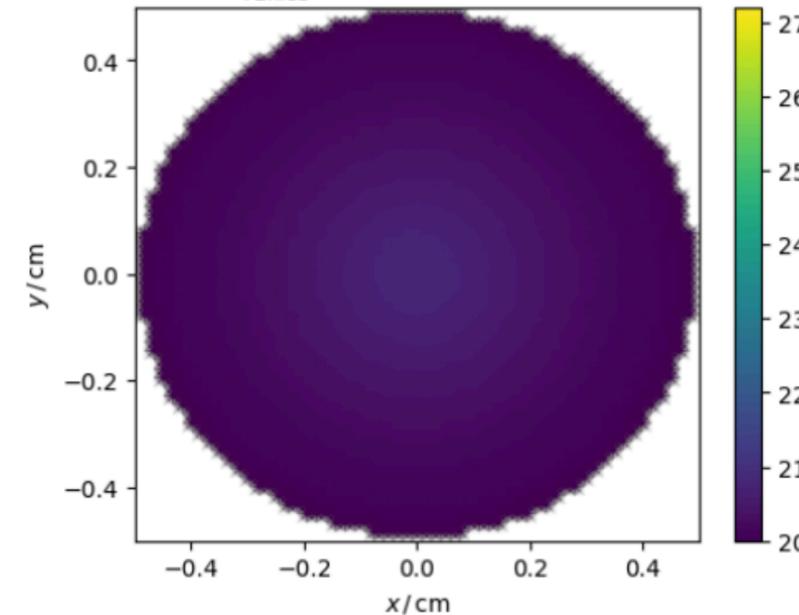
$T_{\text{FEniCS}} / ^\circ\text{C}$ at ($z = 0.62$ cm)



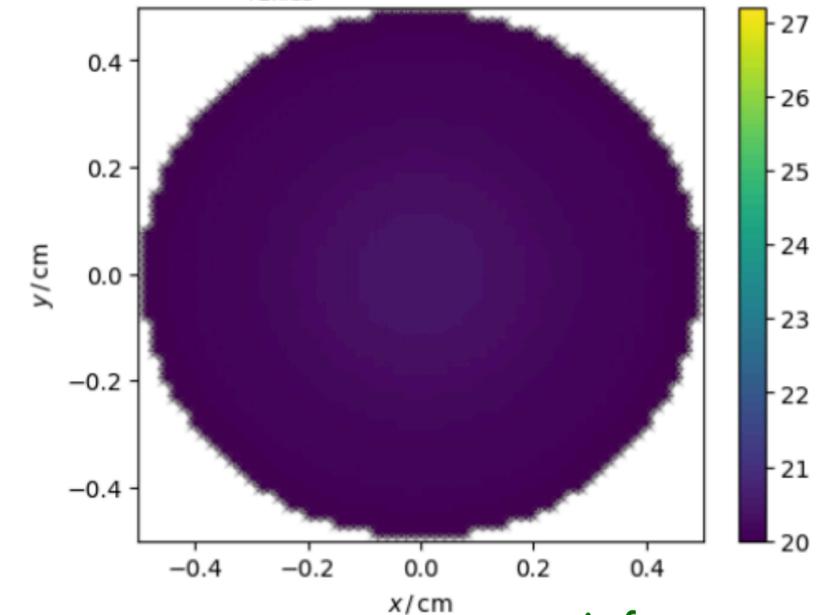
$T_{\text{FEniCS}} / ^\circ\text{C}$ at ($z = 1.25$ cm)



$T_{\text{FEniCS}} / ^\circ\text{C}$ at ($z = 1.88$ cm)



$T_{\text{FEniCS}} / ^\circ\text{C}$ at ($z = 2.50$ cm)



exit face

Lessons Learned, and Next Steps:

Lessons Learned:

- Obtain thermal data characteristic of *your* crystal.
- At room temperature and present power levels, the linear heat equation appears adequate. But ... know / determine your thermal diffusivity, as well as other thermodynamic data.

Next Steps:

- Explore effects at cryogenic temperatures, where α varies more rapidly with temperature.
- Include anisotropic heat conduction — *i.e.* non-axisymmetric (astigmatic) thermal lensing.
- Investigate thermal expansion — *i.e.* additional lensing from thermally induced curvature.

See also the following Jupyter notebook, which you can use on RadiaSoft's Jupyter server:

<https://github.com/radiasoft/rslaser/blob/master/examples/thermal/NLThermalSaturation.ipynb>

Thank you!

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<https://sirepo.com/>

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